

WELLINGTON NORTH SOLAR PLANT

Construction & Operational Noise & Vibration Assessment

10 August 2018

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Important Disclaimer:

The work presented in this document was carried out in accordance with the Renzo Tonin & Associates Quality Assurance System, which is based on Australian Standard / NZS ISO 9001.

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In preparing this report, we have relied upon, and presumed accurate, any information (or confirmation of the absence thereof) provided by the Client and/or from other sources. Except as otherwise stated in the report, we have not attempted to verify the accuracy or completeness of any such information. If the information is subsequently determined to be false, inaccurate or incomplete then it is possible that our observations and conclusions as expressed in this report may change.

We have derived data in this report from information sourced from the Client (if any) and/or available in the public domain at the time or times outlined in this report. The passage of time, manifestation of latent conditions or impacts of future events may require further examination and re-evaluation of the data, findings, observations and conclusions expressed in this report.

We have prepared this report in accordance with the usual care and thoroughness of the consulting profession, for the sole purpose described above and by reference to applicable standards, guidelines, procedures and practices at the date of issue of this report. For the reasons outlined above, however, no other warranty or guarantee, whether expressed or implied, is made as to the data, observations and findings expressed in this report, to the extent permitted by law.

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Contents

1	Intro	oduction	6
2	Proj	ect Description	7
	2.1	Background Information	7
	2.2	Regulatory Requirements	7
	2.3	Receiver Locations	7
	2.4	Hours of Operation	8
		2.4.1 Construction	8
		2.4.2 Operation	g
3	Exis	ting Noise Environment	11
	3.1	Noise Monitoring Locations	11
	3.2	Existing Background & Ambient Noise Levels	11
4	Con	struction Noise Assessment	13
	4.1	Construction Noise Management Levels	13
		4.1.1 Residential Receivers	13
		4.1.2 Sensitive Land Uses	14
	4.2	Construction Noise Sources	15
	4.3	Construction Noise Assessment	16
	4.4	Cumulative Construction Noise Assessment	19
	4.5	Construction Noise Mitigation and Management Measures	22
		4.5.1 General Engineering Noise Controls	23
		4.5.2 Noise Management Measures	24
5	Оре	erational Noise Assessment	26
	5.1	Operational Noise Criteria	26
		5.1.1 Intrusive Noise Impacts	26
		5.1.2 Protecting Noise Amenity	26
	5.2	Summary of Project Noise Trigger Levels	27
	5.3	Operational Noise Sources	28
	5.4	'Modifying Factor' Adjustments	29
	5.5	Operational Noise Assessment	30
	5.6	Cumulative Operation Noise Assessment	32
	5.7	Sleep Disturbance Assessment	34
6	Vibr	ration Assessment	35
	6.1	Vibration Criteria	35
	6.2	Potential Vibration Impacts	37
7	Roa	d Traffic Noise Assessment	39
	7.1	Road Traffic Noise Criteria	39

	7.2	Predicted Road Traffic Noise	40
8	Conc	nclusion	41
APPE	NDIX	IX A Glossary of Terminology	42
APPE	NDIX	X B Long-Term Noise Monitoring Methodology	44
	B.1	Noise Monitoring Equipment	44
	B.2	Meteorology During Monitoring	44
	B.3	Noise vs Time Graphs	44
APPE	NDIX	X C Long Term Noise Monitoring Results	45
List	of ta	ables	
Table	3.1 –	– Measured Existing Background (L ₉₀) & Ambient (L _{eq}) Noise Levels, dB(A)	12
Table	3.2 –	– Rating Background Noise Level, dB(A)	12
Table	4.1 –	- Noise Management Levels (NML) at Residential Receivers, dB(A)	14
Table	4.2 –	- Construction Noise Management Levels (NML) at Residential Receivers, dB(A) 14
Table	4.3 –	- Noise Management Levels (NML) at Other Noise Sensitive Land Uses, dB(A)	15
Table	4.4 –	– Typical Solar Plant Construction Plant & Equipment & Sound Power Levels,	dB(A) 15
Table	4.5 –	– Easement Construction Plant & Equipment & Sound Power Levels, dB(A)	15
Table	4.6 –	– Predicted L _{Aeq,15min} Solar Plant Construction Noise Levels at Receiver Location	ons, dB(A) 17
Table	4.7 –	– Predicted $L_{Aeq,15min}$ East Easement Construction Noise Levels at Receiver Loc	ations, dB(A) 18
Table	4.8 –	– Predicted $L_{Aeq,15min}$ West Easement Construction Noise Levels at Receiver Lo	cations, dB(A) 18
Table		– Predicted $L_{Aeq,15min}$ Cumulative Plant Construction Noise Levels from North a dB(A)	and South Solar Plants, 21
Table	4.10 -	0 – Predicted $L_{Aeq,15min}$ Cumulative Construction Noise Levels from South Solar Easement, dB(A)	Plant and East
Table	4.11 -	 1 – Predicted L_{Aeq,15min} Cumulative Construction Noise Levels from South Solar Easement, dB(A) 	Plant and West 21
Table	4.12 -	2 – Relative Effectiveness of Various Forms of Noise Control, dB(A)	23
Table	4.13 -	3 – Noise Control Measures for Likely Construction Plant	23
Table	5.1 –	– NPfl Intrusive Noise Level at Residential Receivers, dB(A)	26
Table	5.2 –	– NPfl Project Amenity Noise Levels, dB(A)	27
Table	5.3 –	– Project Noise Trigger Levels, dB(A)	28
Table	5.4 –	- Typical Operational Plant and Equipment & Sound Power Levels	29
Table	5.5 –	– Predicted L _{Aeq,15min} Operational Noise Levels at Receiver Locations, dB(A)	31
Table	5.6 –	– Predicted $L_{Aeq,15min}$ Cumulative Operational Noise Levels at Receiver Locatio	ns, dB(A) 33
Table	6.1 –	– Types of Vibration	35
Table	6.2 –	– Preferred and Maximum Levels for Human Comfort	36
Table	6.3 –	– Acceptable Vibration Dose Values for Intermittent Vibration (m/s ^{1.75})	37
Table	6.4 –	– Potential Vibration Impacts for Identified Receivers	37

Table 7.1 – Summary of the Estimated Construction Traffic Volumes During Peak Construction	39
Table 7.2 – RNP Road Traffic Noise Criteria, dB(A)	39
Table 7.3 – Exiting Traffic Volumes Along Campbells Lane	40
Table 7.4 – Predicted Road Traffic Noise Contribution Levels Along Public Roads, dB(A) L _{Aeq(1 Hour)}	40
List of figures	
Figure 1 – Site, Surrounds and Receiver and Noise Monitoring Locations	10
Figure 2 – Orthogonal Axes for Human Exposure to Vibration	36

1 Introduction

Renzo Tonin & Associates was engaged to conduct an environmental noise and vibration assessment of the proposed Wellington North Solar Plant located approximately seven kilometres north east of the town of Wellington in New South Wales as part of the Environmental Impact Statement (EIS) for the project. Noise and vibration impacts from the construction and operation phases of the project will be addressed in this report in accordance with the Secretary's Environmental Assessment Requirements (SEARs).

The work documented in this report was carried out in accordance with the Renzo Tonin & Associates Quality Assurance System, which is based on Australian Standard / NZS ISO 9001. Appendix A contains a glossary of acoustic terms used in this report.

2 Project Description

2.1 Background Information

The Wellington North Solar Plant project includes the construction and operation of a solar photovoltaic (PV) plant and associated infrastructure, with a capacity of approximately 300MW. The subject site is located approximately seven kilometres north east of the town of Wellington in New South Wales, within the Dubbo Regional Council Local Government Area (LGA).

2.2 Regulatory Requirements

Noise and vibration impacts are assessed in accordance with a number of policies, guidelines and standards, including:

- NSW 'Interim Construction Noise Guideline' (ICNG Department of the Environment and Climate Change, 2009);
- NSW 'Noise Policy for Industry' (NPfI Environment Protection Authority, 2017);
- 'Assessing Vibration: A Technical Guideline' (Department of the Environment and Climate Change, 2006); and
- NSW 'Road Noise Policy' (RNP Department of Environment, Climate Change and Water, 2011)

2.3 Receiver Locations

The nearest affected receivers were identified through aerial maps as follows:

- Receiver R1 104 Cobbora Road, Maryvale
 Residential property located approximately 330m south of the project area.
- Receiver R2 215 Cobbora Road, Maryvale
 Residential property located approximately 135m west of the project area.
- Receiver R3 301 Cobbora Road, Maryvale
 Residential property located approximately 315m west of the project area.
- Receiver R4 66 Campbells Lane, Bodangora
 Residential property located approximately 110m north of the project area.
- Receiver R5 6219 Goolma Road, Bodangora
 Residential property located approximately 910m north-east of the project area.
- Receiver R6 Lot 5 DP 664334 Gladstone Road, Bodangora
 Residential property located approximately 255m east of the project area.

•	Receiver R7 –	104 Gladstone Road, Bodangora
		Industrial property located approximately 330m east of the project area

- Receiver R8 Wellington Correction Centre
 Correction centre located approximately 400m east of the project area.
- Receiver R9 28 Cadia Place, Wuuluman
 Residential property located approximately 1,220m south-east of the project area.
- Receiver R10 6582 Goolma Road, Bodangora Soil Conservation Service
 Commercial property located within the project area.
- Receiver R11 152 Bela Vista Lane, Montefiores
 Residential property located approximately 1,300m south of the project area
- Receiver R12 6938 Goolma Road, Montefiores
 Residential property located approximately 1,700m south of the project area
- Receiver R13 7009 Goolma Road, Montefiores
 Residential property located approximately 3,500m south of the project area
- Receiver R14 59 Twelve Mile Road, Wuuluman
 Residential property located approximately 1,600m south of the project area
- Receiver R15 6773 Goolma Road, Wuuluman
 Residential property located approximately 3,300m south of the project area
- Receiver R16 6916 Goolma Road, Wuuluman
 Residential property located approximately 1,200m south of the project area

Figure 1 provides details of the site, surrounds and receiver locations.

2.4 Hours of Operation

2.4.1 Construction

Construction will occur during the following standard hours of construction:

Monday to Friday: 7:00am to 6:00pm

Saturday: 8:00am to 1:00pm

No work on Sundays or public holidays

2.4.2 Operation

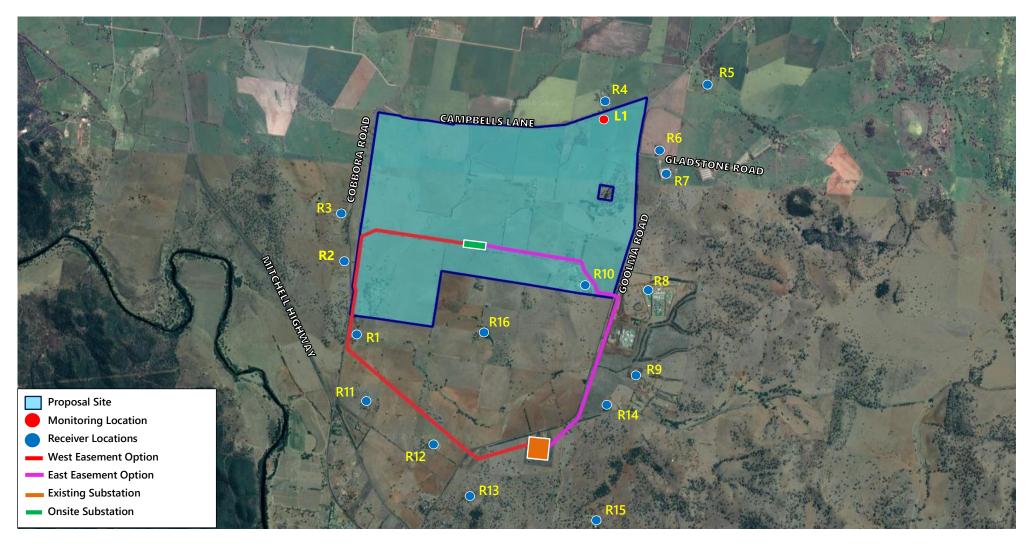
The solar farm will operate autonomously during times when there is sunlight. This will predominantly be during day and evening periods (7am-6pm and 6pm-10pm, respectively) throughout the year and potentially part of the night time period (prior to 7am) during the summer months.

Furthermore, there will be staff on site during the following standard hours:

Monday to Friday: 7:00am to 6:00pm

Saturday: 8:00am to 1:00pm

Figure 1 – Site, Surrounds and Receiver and Noise Monitoring Locations



3 Existing Noise Environment

Background noise varies over the course of any 24 hour period, typically from a minimum at 3am in the morning to a maximum during morning and afternoon traffic peak hours. Therefore, the NSW 'Noise Policy for Industry' (NPfI, 2017) requires that the level of background and ambient noise be assessed separately for the daytime, evening and night-time periods. The NSW NPfI defines these periods as follows:

- Day is defined as 7:00am to 6:00pm, Monday to Saturday and 8:00am to 6:00pm Sundays & Public Holidays.
- Evening is defined as 6:00pm to 10:00pm, Monday to Sunday & Public Holidays.
- **Night** is defined as 10:00pm to 7:00am, Monday to Saturday and 10:00pm to 8:00am Sundays & Public Holidays.

3.1 Noise Monitoring Locations

Noise monitoring is to be undertaken at the nearest or potentially most affected receiver locations; or if this is not available, then at a location considered to have a noise environment representative of the nearest or potentially most affected receiver locations. In this case the representative location where noise monitoring was undertaken was as follows.

Location L1 – Coordinates: -32°29'0.48", 148°58'26.84" (near Receiver R4)
 Noise monitor was installed in the 'free field' (ie. away from building facades) on the north eastern corner of the subject site. Noise data represents the background and ambient noise environment for receivers surrounding the project area.

To quantify the existing ambient noise environment, long-term (unattended) noise monitoring was conducted at Location L1 between Thursday 5th October and Thursday 12th October 2017.

Appendix A of this report presents a description of noise terms. Appendix B details the noise monitoring methodology and the graphical recorded outputs from long term noise monitoring are included in Appendix C. The graphs in Appendix C were analysed to determine an assessment background level (ABL) for each day, evening and night period in each 24 hour period of noise monitoring, and based on the median of individual ABLs an overall single Rating Background Level (RBL) for the day, evening and night period is determined over the entire monitoring period in accordance with the NSW NPfl.

3.2 Existing Background & Ambient Noise Levels

Existing background and ambient noise levels are presented in Table 3.1 below. The noise monitor was positioned outdoors in the 'free-field' (ie. away from building facades). Construction and operation

noise from the site should be assessed away from the facade at the potentially most affected residential boundaries and therefore, the representative noise levels listed in Table 3.1 are directly applicable.

Table 3.1 – Measured Existing Background (L₉₀) & Ambient (L_{eq}) Noise Levels, dB(A)

Lacation	L ₉₀ Background Noise Levels			L _{eq} Ambient Noise Levels		
Location	Day	Evening	Night	Day	Evening	Night
L1 (-32°29'0.48", 148°58'26.84")	27	34	26	49	46	47

The identified receivers surrounding the subject site are all classified as rural under NPfl guidelines. It was found that the background noise levels were typical for a rural area, with a day RBL less than 40dB(A), an evening RBL of 35 dB(A) and a night RBL less than 30 dB(A).

Based on Table 2.1 on page 10 of the NPfl, where background noise levels are less than the minimum assumed RBLs, the minimum assumed RBL's are adopted instead for all receiver locations nominated in Section 2.3. Therefore, the background noise levels have been set at the levels detailed in the fourth column of Table 3.2 below.

Table 3.2 – Rating Background Noise Level, dB(A)

Time of Day	Measured Existing Background (L∞), dB(A)	Minimum Assumed RBLs, dB(A) ¹	Applicable Rating Background Level, dB(A)
Day	27	35	35
Evening	34	30	34
Night	26	30	30

Notes: 1. In accordance with Table 2.1 of the NSW NPfI

4 Construction Noise Assessment

4.1 Construction Noise Management Levels

The NSW 'Interim Construction Noise Guideline' (ICNG, 2009) provides guidelines for assessing noise generated during the construction phase of developments.

The key components of the guideline that are incorporated into this assessment include:

Use of L_{Aeq} as the descriptor for measuring and assessing construction noise

NSW noise policies, including the NPfI, RNP and RING have moved to the primary use of L_{Aeq} over any other descriptor. As an energy average, L_{Aeq} provides ease of use when measuring or calculating noise levels since a full statistical analysis is not required as when using, for example, the L_{A10} descriptor.

Application of reasonable and feasible noise mitigation measures

As stated in the ICNG, a noise mitigation measure is feasible if it is capable of being put into practice and is practical to build given the project constraints.

Selecting reasonable mitigation measures from those that are feasible involves making a judgement to determine whether the overall noise benefit outweighs the overall social, economic and environmental effects.

The ICNG provides two methods for assessment of construction noise, being either a quantitative or a qualitative assessment. A quantitative assessment is recommended for major construction projects of significant duration, and involves the measurement and prediction of noise levels, and assessment against set criteria. A qualitative assessment is recommended for small projects with duration of less than three weeks and focuses on minimising noise disturbance through the implementation of reasonable and feasible work practices, and community notification.

Given the length of the construction works proposed, a quantitative assessment is carried out herein, consistent with the ICNG requirements.

4.1.1 Residential Receivers

Table 4.1 reproduced from the ICNG, sets out the noise management levels and how they are to be applied for residential receivers.

Table 4.1 - Noise Management Levels (NML) at Residential Receivers, dB(A)

Time of Day	Management Level L _{Aeq (15 min)}	How to Apply
Recommended standard hours: Monday to Friday 7 am to 6 pm Saturday 8 am to 1 pm No work on Sundays or public holidays	Noise affected RBL + 10dB(A)	The noise affected level represents the point above which there may be some community reaction to noise. Where the predicted or measured LAeq (15 min) is greater than the noise affected level, the proponent should apply all feasible and reasonable work practices to meet the noise affected level. The proponent should also inform all potentially impacted residents of the nature of works to be carried out, the expected noise levels and duration, as well as contact details.
	Highly noise affected 75dB(A)	The highly noise affected level represents the point above which there may be strong community reaction to noise. Where noise is above this level, the relevant authority (consent, determining or regulatory) may require respite periods by restricting the hours that the very noisy activities can occur, taking into account: • times identified by the community when they are less sensitive to noise (such as before and after school for works near schools, or mid-morning or mid-afternoon for works near residences) • if the community is prepared to accept a longer period of construction in exchange for restrictions on construction times.
Outside recommended standard hours	Noise affected RBL + 5dB(A)	A strong justification would typically be required for works outside the recommended standard hours. The proponent should apply all feasible and reasonable work practices to meet the noise affected level. Where all feasible and reasonable practices have been applied and noise is more than 5dB(A) above the noise affected level, the proponent should negotiate with the community. For guidance on negotiating agreements see section 7.2.2 of the ICNG.

Table 4.2 presents the construction noise management levels established for the nearest noise sensitive residential receivers based upon the noise monitoring results presented in Table 3.1, the proposed construction hours and the above ICNG requirements. The receiver locations are marked in Figure 1.

Table 4.2 - Construction Noise Management Levels (NML) at Residential Receivers, dB(A)

Location Description	Day L _{A90} Background Noise Level (RBL)	Day Noise Management Level L _{Aeq(15min)}
All residential receivers	35 ¹	45
(Receivers R1-R6 & R9 & R11-R16)	33	43

Notes: 1. Construction works occur during the daytime period only; hence, only the day period is assessed

4.1.2 Sensitive Land Uses

Table 4.3 sets out the ICNG noise management levels for other types of noise sensitive receiver locations applicable for this project.

Table 4.3 - Noise Management Levels (NML) at Other Noise Sensitive Land Uses, dB(A)

Land Use	Where Objective Applies	Management Level Laeq (15 Min)
Receiver R7 – 104 Gladstone Rd, Bodangora (industrial receiver)	External noise level	75dB(A)
Receiver R8 – Wellington Correctional Centre (commercial receiver)	External noise level	70dB(A)
Receiver R10 – Soil Conservation Service (commercial receiver)	External noise level	70dB(A)

Notes: 1. Noise Management Levels only apply when premises are in use

4.2 Construction Noise Sources

Table 4.4 lists typical plant and equipment likely to be used by the contractor to carry out the necessary construction works within the proposal site depicted in Figure 1, while Table 4.5 details the equipment required to construct the easements for the project.

Table 4.4 – Typical Solar Plant Construction Plant & Equipment & Sound Power Levels, dB(A)

Plant Item	Plant Description	Number of Items	L _{Aeq} Sound Power Levels, dB(A) re. 1pW Single Item
1	Small pile driving rig	10	114
2	Crane	4	110
3	Drum roller	4	109
4	Padfoot roller	4	109
5	Wheeled loader	3	109
6	Dump truck	6	108
7	30t Excavator	10	107
8	Grader	6	107
9	Chain trencher	4	104
10	Water truck	4	104
11	Telehandler	4	98
12	Forklift	4	90

Table 4.5 – Easement Construction Plant & Equipment & Sound Power Levels, dB(A)

Plant Item	Plant Description	Number of Items	L _{Aeq} Sound Power Levels, dB(A) re. 1pW Single Item
1	Crane	1	110
2	Dump truck	1	108
3	30t Excavator	1	107
4	Grader	1	107
5	Chain trencher	1	104
6	Water truck	1	104

The sound power levels for the majority of activities presented in the above table are provided by the client, based on maximum levels given in Table A1 of Australian Standard 2436 - 2010 'Guide to Noise Control on Construction, Demolition and Maintenance Sites', the ICNG, information from past projects and/or information held in our library files.

4.3 Construction Noise Assessment

Noise emissions were predicted by modelling the noise sources, receiver locations, topographical features of the intervening area, and possible noise control treatments using CadnaA (version 2018) noise modelling computer program. The program calculates the contribution of each noise source at each specified receptor point and allows for the prediction of the total noise from a site.

The noise prediction models takes into account:

- Location of noise sources and receiver locations;
- Height of sources and receivers;
- Separation distances between sources and receivers;
- Ground type between sources and receivers (soft); and
- Attenuation from barriers (natural and purpose built).

Noise levels at any receptors resulting from construction would depend on the above and the type and duration of construction being undertaken. Furthermore, noise levels at receivers would vary substantially over the total construction program due to the transient nature and large range of plant and equipment that could be used.

Table 4.6 presents construction noise levels likely to be experienced at the nearby affected receivers based on the construction activities and plant equipment associated with the works conducted within the proposal site. Table 4.7 and Table 4.8 refer to the noise levels likely to be experienced at the nearby affected receivers due to the construction of the easements. The noise level ranges represent the noise source being located at the furthest to the closest proximity to each receiver location.

10 AUGUST 2018 RENZO TONIN & ASSOCIATES

Table 4.6 – Predicted L_{Aeq,15min} Solar Plant Construction Noise Levels at Receiver Locations, dB(A)

Plant	Diana Daganinatian							Predicted L	eq(15min) Con	struction N	oise Levels						
Item	Plant Description	R1	R2	R3	R4	R5	R6	R7	R8	R9	R10	R11	R12	R13	R14	R15	R16
Noise Mo	anagement Level ¹	45	45	45	45	45	45	75³	70 ²	45	70 ²	45	45	45	45	45	45
1	Small pile driving rig	<20-39	<20- 49	<20-42	<20 -47	<20-31	<20-44	<20-40	<20-40	<20-29	<20-57	<20-28	<20-25	<20-20	<20-26	<20-<20	<20-34
2	Crane	<20-35	<20-45	<20-38	<20-43	<20-27	<20-40	<20-36	<20-36	<20-25	<20-53	<20-24	<20-21	<20-<20	<20-22	<20-<20	<20-30
3	Drum roller	<20-34	<20-44	<20-37	<20-42	<20-26	<20-39	<20-35	<20-35	<20-24	<20-52	<20-23	<20-20	<20-<20	<20-21	<20-<20	<20-29
4	Padfoot roller	<20-34	<20-44	<20-37	<20-42	<20-26	<20-39	<20-35	<20-35	<20-24	<20-52	<20-23	<20-20	<20-<20	<20-21	<20-<20	<20-29
5	Wheeled loader	<20-34	<20-44	<20-37	<20-42	<20-26	<20-39	<20-35	<20-35	<20-24	<20-52	<20-23	<20-20	<20-<20	<20-21	<20-<20	<20-29
6	Dump truck	<20-33	<20-43	<20-36	<20-41	<20-25	<20-38	<20-34	<20-34	<20-23	<20-51	<20-22	<20-<20	<20-<20	<20-<20	<20-<20	<20-28
7	30t Excavator	<20-32	<20-42	<20-35	<20-40	<20-24	<20-37	<20-33	<20-33	<20-22	<20-50	<20-21	<20-<20	<20-<20	<20-<20	<20-<20	<20-27
8	Grader	<20-32	<20-42	<20-35	<20-40	<20-24	<20-37	<20-33	<20-33	<20-22	<20-50	<20-21	<20-<20	<20-<20	<20-<20	<20-<20	<20-27
9	Chain trencher	<20-29	<20-39	<20-32	<20-37	<20-21	<20-34	<20-30	<20-30	<20-<20	<20-47	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-24
10	Water truck	<20-29	<20-39	<20-32	<20-37	<20-21	<20-34	<20-30	<20-30	<20-<20	<20-47	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-24
11	Telehandler	<20-23	<20-33	<20-26	<20-31	<20-<20	<20-28	<20-24	<20-24	<20-<20	<20-41	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20
12	Forklift	<20-<20	<20-25	<20-<20	<20-23	<20-<20	<20-20	<20-<20	<20-<20	<20-<20	<20-33	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20
•	(noisiest) plant g concurrently	<20-41	<20- 51	<20-45	<20-49	<20-33	<20- 46	<20-42	<20-42	<20-31	<20-59	<20-31	<20-28	<20-23	<20-28	<20-<20	<20-36

Notes: 1. Noise Management Levels for day period (ie. standard construction hours)

^{2.} Noise Management Level for commercial type premises

^{3.} Noise Management Level for industrial type premises

^{4.} Bold font represents exceedance of the relevant NML

Table 4.7 – Predicted L_{Aeq,15min} East Easement Construction Noise Levels at Receiver Locations, dB(A)

Plant	No. 1 Dec. 1 dec.							Predicted L	eq(15min) Con	struction N	oise Levels						
Item	Plant Description	R1	R2	R3	R4	R5	R6	R7	R8	R9	R10	R11	R12	R13	R14	R15	R16
Noise	Management Level ¹	45	45	45	45	45	45	75³	70 ²	45	70 ²	45	45	45	45	45	45
1	Crane	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-21	<20-37	<20-32	<20-54	<20-<20	<20-22	<20-24	<20-38	<20-26	<20-25
2	Dump truck	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-35	<20-30	<20-52	<20-<20	<20-<20	<20-22	<20-36	<20-24	<20-23
3	30t Excavator	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-34	<20-29	<20-51	<20-<20	<20-<20	<20-21	<20-35	<20-23	<20-22
4	Grader	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-34	<20-29	<20-51	<20-<20	<20-<20	<20-21	<20-35	<20-23	<20-22
5	Chain trencher	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-31	<20-26	<20-48	<20-<20	<20-<20	<20-<20	<20-32	<20-20	<20-<20
6	Water truck	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-31	<20-26	<20-48	<20-<20	<20-<20	<20-<20	<20-32	<20-20	<20-<20
•	3 (noisiest) plant ting concurrently	<20-21	<20-23	<20-22	<20-20	<20-<20	<20-23	<20-24	<20-40	<20-35	21-58	<20-<20	<20-25	<20-28	<20-41	<20-29	23-28

Notes: 1. Noise Management Levels for day period (ie. standard construction hours)

2. Noise Management Level for commercial type premises

3. Noise Management Level for industrial type premises

Table 4.8 – Predicted L_{Aeq,15min} West Easement Construction Noise Levels at Receiver Locations, dB(A)

Plant	Plant							Predicted I	eq(15min) Con	struction N	oise Levels						
Item	Description	R1	R2	R3	R4	R5	R6	R7	R8	R9	R10	R11	R12	R13	R14	R15	R16
Noise M	anagement Level ¹	45	45	45	45	45	45	75³	70 ²	45	70 ²	45	45	45	45	45	45
1	Crane	<20- 52	<20- 46	<20-37	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-21	<20-20	<20-35	<20-42	<20-34	<20-25	<20-24	<20-25
2	Dump truck	<20- 50	<20-44	<20-35	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-33	<20-40	<20-32	<20-23	<20-22	<20-23
3	30t Excavator	<20- 49	<20-43	<20-34	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-32	<20-39	<20-31	<20-22	<20-21	<20-22
4	Grader	<20- 49	<20-43	<20-34	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-32	<20-39	<20-31	<20-22	<20-21	<20-22
5	Chain trencher	<20- 46	<20-40	<20-31	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-29	<20-36	<20-28	<20-<20	<20-<20	<20-<20
6	Water truck	<20- 46	<20-40	<20-31	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-29	<20-36	<20-28	<20-<20	<20-<20	<20-<20
•	(noisiest) plant ng concurrently	<20- 55	<20- 50	<20-40	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-24	<20-24	<20-38	<20-45	<20-37	<20-29	<20-28	21-28

Notes: 1. Noise Management Levels for day period (ie. standard construction hours)

2. Noise Management Level for commercial type premises

3. Noise Management Level for industrial type premises

4. **Bold** font represents exceedance of the relevant NML

Based on the construction noise levels presented in Table 4.6 the construction management levels at Receivers R2, R4 and R6 may be exceeded when construction works are conducted at closest proximity to the receivers. For the east easement option, Table 4.7 indicates that construction noise would not exceed at any receiver locations. For the west easement option, Table 4.8 indicates that the construction noise management levels at Receivers R1 and R2 may also be exceeded. It is noted that construction noise levels at all receivers are predicted to be less than the highly noise affected level of 75dB(A) for all construction stages of the solar farm project.

In light of the predicted noise levels above, it is recommended that a feasible and reasonable approach towards noise management measures be applied to reduce noise levels as much as possible to manage the impact from construction noise.

Further details on construction noise mitigation and management measures are provided in Section 4.5 below.

4.4 Cumulative Construction Noise Assessment

Construction activities associated with the recently approved Wellington Solar Plant (Wellington South Solar Plant) may potentially occur at the same time as construction works required for the proposed Wellington North Solar Plant. As a result, some of the nominated receivers may be impacted by construction noise from both solar plants concurrently. Therefore, a cumulative construction noise assessment has been undertaken for the scenario where both solar plants are being constructed at the same time; however, it is highly unlikely the two solar plants will be constructed concurrently due to the different timelines of the projects and the timing of approvals.

The construction and operation noise and vibration assessment for the Wellington South Solar Plant was previously prepared by Renzo Tonin & Associates [ref: TJ643-01F01 Report (r5), dated 24 November 2017], which identified nearby receivers potentially impacted by construction noise.

The following assessment assumes that the same construction plant and equipment are being used at both solar plants concurrently during the construction of the solar plants. Furthermore, the construction of the Wellington South Solar Plant concurrently with each of the easement options have also been assessed.

From the comparison of Table 4.4 and Table 4.5, it is evident that the typical plant and equipment used to construct the solar plant slightly differ to the plant and equipment used for the construction of the easements. Therefore, for the scenario where the easements are constructed concurrently with the Wellington South Solar Plant, a conservative approach has been taken, where it is assumed that the three (3) noisiest plant items from each work site are operating concurrently.

Table 4.9 presents cumulative construction noise levels likely to be experienced at the nearby affected receivers based on the concurrent construction of the Wellington North and Wellington South Solar Plants. Similarly, Table 4.10 and Table 4.11 present the cumulative construction noise levels for the scenario where each of the easements associated with the Wellington North Solar Plant are constructed concurrently with the Wellington South Solar Plant.

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Table 4.9 – Predicted L_{Aeq,15min} Cumulative Plant Construction Noise Levels from North and South Solar Plants, dB(A)

Plant	Diant Dannintian												Predic	ted L _{eq(15mir}) Construct	tion Noise	Levels											
Item	Plant Description		R1			R2			R8			R9			R10			R11			R12			R13			R14	
Noise N	Management Level ¹		45			45			70 ²			45			70 ²			45			45			45			45	
	Work Areas	South	North	Cumul. ³	South	North	Cumul. ³	South	North	Cumul. ³	South	North	Cumul. ³	South	North	Cumul. ³	South	North	Cumul. ³	South	North	Cumul. ³	South	North	Cumul. ³	South	North	Cumul. ³
1	Small pile driving rig	23- 47	<20-39	23- 47	23-34	<20- 49	23- 49	23-42	<20-40	23-44	23-36	<20-29	23-37	21-45	<20-57	22-57	23-31	<20-28	23-33	23-38	<20-25	23-38	23-36	<20-20	23-36	23-42	<20-26	23-42
2	Crane	<20-43	<20-35	<20-43	<20-30	<20-45	<20-45	<20-38	<20-36	<20-40	<20-32	<20-25	<20-33	<20-41	<20-53	<20-53	<20-27	<20-24	<20-29	<20-34	<20-21	<20-34	<20-32	<20-<20	<20-32	<20-38	<20-22	<20-38
3	Drum roller	<20-42	<20-34	<20-42	<20-29	<20-44	<20-44	<20-37	<20-35	<20-39	<20-31	<20-24	<20-32	<20-40	<20-52	<20-52	<20-26	<20-23	<20-28	<20-33	<20-20	<20-33	<20-31	<20-<20	<20-31	<20-37	<20-21	<20-37
4	Padfoot roller	<20-42	<20-34	<20-42	<20-29	<20-44	<20-44	<20-37	<20-35	<20-39	<20-31	<20-24	<20-32	<20-40	<20-52	<20-52	<20-26	<20-23	<20-28	<20-33	<20-20	<20-33	<20-31	<20-<20	<20-31	<20-37	<20-21	<20-37
5	Wheeled loader	<20-42	<20-34	<20-42	<20-29	<20-44	<20-44	<20-37	<20-35	<20-39	<20-31	<20-24	<20-32	<20-40	<20-52	<20-52	<20-26	<20-23	<20-28	<20-33	<20-20	<20-33	<20-31	<20-<20	<20-31	<20-37	<20-21	<20-37
6	Dump truck	<20-41	<20-33	<20-41	<20-28	<20-43	<20-43	<20-36	<20-34	<20-38	<20-30	<20-23	<20-31	<20-39	<20-51	<20-51	<20-25	<20-22	<20-27	<20-32	<20-<20	<20-32	<20-30	<20-<20	<20-30	<20-36	<20-20	<20-36
7	30t Excavator	<20-40	<20-32	<20-40	<20-27	<20-42	<20-42	<20-35	<20-33	<20-37	<20-29	<20-22	<20-30	<20-38	<20-50	<20-50	<20-24	<20-21	<20-26	<20-31	<20-<20	<20-31	<20-29	<20-<20	<20-29	<20-35	<20-<20	<20-35
8	Grader	<20-40	<20-32	<20-40	<20-27	<20-42	<20-42	<20-35	<20-33	<20-37	<20-29	<20-22	<20-30	<20-38	<20-50	<20-50	<20-24	<20-21	<20-26	<20-31	<20-<20	<20-31	<20-29	<20-<20	<20-29	<20-35	<20-<20	<20-35
9	Chain trencher	<20-37	<20-29	<20-37	<20-24	<20-39	<20-39	<20-32	<20-30	<20-34	<20-26	<20-<20	<20-27	<20-35	<20-47	<20-47	<20-21	<20-<20	<20-23	<20-28	<20-<20	<20-28	<20-26	<20-<20	<20-26	<20-32	<20-<20	<20-32
10	Water truck	<20-37	<20-29	<20-37	<20-24	<20-39	<20-39	<20-32	<20-30	<20-34	<20-26	<20-<20	<20-27	<20-35	<20-47	<20-47	<20-21	<20-<20	<20-23	<20-28	<20-<20	<20-28	<20-26	<20-<20	<20-26	<20-32	<20-<20	<20-32
11	Telehandler	<20-31	<20-23	<20-31	<20-<20	<20-33	<20-33	<20-26	<20-24	<20-28	<20-20	<20-<20	<20-21	<20-29	<20-41	<20-41	<20-<20	<20-<20	<20-<20	<20-22	<20-<20	<20-22	<20-20	<20-<20	<20-20	<20-26	<20-<20	<20-26
12	Forklift	<20-23	<20-<20	<20-23	<20-<20	<20-25	<20-25	<20-<20	<20-<20	<20-20	<20-<20	<20-<20	<20-<20	<20-21	<20-33	<20-33	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20	<20-<20
-	(noisiest) plant ng concurrently	25- 49	<20-41	26- 50	25-36	<20- 51	26- 51	25-44	<20-42	26-46	25-39	<20-31	26-39	23-47	<20-59	24-60	25-33	<20-31	26-35	25-40	<20-28	26-41	25-39	<20-23	26-39	25-44	<20-28	26-44

Notes: 1. Noise Management Levels for day period (ie. standard construction hours)

2. Noise Management Level for commercial type premises

3. Overall noise contribution from construction noise from South and North Solar Plants

4. **Bold** font represents exceedance of the relevant NML

Table 4.10 – Predicted L_{Aeq,15min} Cumulative Construction Noise Levels from South Solar Plant and East Easement, dB(A)

Plant Plant Description												Predic	ted Leq(15min	n) Construc	tion Noise	Levels											
Item		R1			R2			R8			R9			R10			R11			R12			R13			R14	
Noise Management Level ¹		45			45			70 ²			45			70 ²			45			45			45			45	
Work Areas	South	East	Cumul. ³	South	East	Cumul. ³	South	East	Cumul. ³	South	East	Cumul. ³	South	East	Cumul. ³	South	East	Cumul. ³	South	East	Cumul. ³	South	East	Cumul. ³	South	East	Cumul. ³
Up to 3 (noisiest) plant operating concurrently ⁴	25- 49	<20-21	26- 49	25-36	<20-23	26-36	25-44	<20-40	26-46	25-39	<20-35	26-43	23-47	21-58	25-58	25-33	<20-<20	26-33	25-40	<20-25	26-40	25-39	<20-28	26-39	25-44	<20-41	26- 46

Notes: 1. Noise Management Levels for day period (ie. standard construction hours)

2. Noise Management Level for commercial type premises

3. Overall noise contribution from construction noise from South Solar Plant and North Solar Plant's associated east easement

4. Up to 3 noisiest plant of each work area operating concurrently

5. **Bold** font represents exceedance of the relevant NML

Table 4.11 – Predicted L_{Aeq,15min} Cumulative Construction Noise Levels from South Solar Plant and West Easement, dB(A)

Plant Description												Predic	ted L _{eq(15mir}	n) Construc	tion Noise	Levels											
Item Plant Description		R1			R2			R8			R9			R10			R11			R12			R13			R14	
Noise Management Level ¹		45			45			70 ²			45			70 ²			45			45			45			45	
Work Areas	South	West	Cumul. ³	South	West	Cumul. ³	South	West	Cumul. ³	South	West	Cumul. ³	South	West	Cumul. ³	South	West	Cumul. ³	South	West	Cumul. ³	South	West	Cumul. ³	South	West	Cumul. ³
Up to 3 (noisiest) plant operating concurrently	25- 49	<20- 55	26- 56	25-36	<20- 50	26- 50	25-44	<20-<20	26-44	25-39	<20-24	25-39	23-47	<20-24	23-47	25-33	<20-38	26-39	25-40	<20-45	26- 46	25-39	<20-37	26-41	25-44	<20-29	26-44

Notes: 1. Noise Management Levels for day period (ie. standard construction hours)

2. Noise Management Level for commercial type premises

3. Overall noise contribution from construction noise from South Solar Plant and North Solar Plant's associated west easement

4. Up to 3 noisiest plant of each work area operating concurrently

5. **Bold** font represents exceedance of the relevant NML

The results presented in Table 4.9 indicate exceedances above the NML for Receivers R1 and R2. The exceedance at Receiver R1 is mainly due to the construction of the South Solar Plant, which was initially identified as exceeding the NML in the Wellington South Solar Plant's noise and vibration assessment [ref: TJ643-01F01 Report (r5), dated 24 November 2017]. The construction of the North Solar Plant is the main contributor to the exceedance at Receiver R2, which has been identified in Section 4.3. Therefore, the predicted cumulative noise impact from the construction of both solar plants does not identify any new exceedances at nearby affected receivers.

For the cumulative construction noise levels of the North Solar Plant's eastern easement and the South Solar Plant construction works, Receivers R1 and R14 exceed the NML. The exceedance at Receiver R1 is only due to the construction works from the South Solar Plant, while the exceedance at R14 only occurs when the three (3) noisiest plant and equipment are operating at the closest proximity to the receiver from each work site.

Similarly, the cumulative construction of the North Solar Plant's western easement and the South Solar Plant exceed the NML at Receivers R1, R2 and R12. The construction noise from the western easement and the South Solar Plant both contribute to the exceedance at R1. The exceedance at R2 is caused by the construction works from the western easement. When the concurrent construction of the North Solar Plant's western easement and the South Solar Plant occur at the closest proximity to receiver R12 it is predicted to exceed the NML.

The probability of the scenario, where the South Solar Plant, and either of the North Solar Plant's easements are constructed concurrently and have their three (3) noisiest plant equipment operating at the closest proximity to the affected receivers, is generally low. However, if it were to occur it is recommended that a feasible and reasonable approach towards noise management measures should be applied to reduce the noise levels as much as possible to manage the impact from the cumulative construction noise.

Additionally, the cumulative construction noise levels of the South Solar Plant and the North Solar Plant, and it's associated easements, are predicted to be less than the highly noise affected level of 75dB(A), as shown in Table 4.9, Table 4.10 and Table 4.11.

4.5 Construction Noise Mitigation and Management Measures

The following recommendations provide in-principle feasible and reasonable noise control solutions to reduce noise impacts to sensitive receivers. Where actual construction activities differ from those assessed in this report, more detailed design of noise control measures may be required once specific items of plant and construction methods have been chosen and assessed on site.

The advice provided here is in respect of acoustics only. Supplementary professional advice may need to be sought in respect of fire ratings, structural design, buildability, fitness for purpose and the like.

4.5.1 General Engineering Noise Controls

Implementation of noise control measures, such as those suggested in Australian Standard 2436-2010 "Guide to Noise Control on Construction, Demolition and Maintenance Sites", are expected to reduce predicted construction noise levels. Reference to Australian Standard 2436-2010, Appendix C, Table C1 suggests possible remedies and alternatives to reduce noise emission levels from typical construction equipment. Table C2 in Appendix C presents typical examples of noise reductions achievable after treatment of various noise sources. Table C3 in Appendix C presents the relative effectiveness of various forms of noise control treatment.

Table 4.12 below presents noise control methods, practical examples and expected noise reductions according to AS2436 and according to Renzo Tonin & Associates' opinion based on experience with past projects.

Table 4.12 - Relative Effectiveness of Various Forms of Noise Control, dB(A)

Noise Control	Drostical Communica		oise Reduction e in Practice		Noise Reduction e in Practice
Method	Practical Examples -	AS 2436	Renzo Tonin & Associates	AS 2436	Renzo Tonin & Associates
Distance	Doubling of distance between source and receiver	6	6	6	6
Screening	Acoustic barriers such as earth mounds, temporary or permanent noise barriers	5 to 10	5 to 10	15	15
Acoustic Enclosures	Engine casing lagged with acoustic insulation and plywood	15 to 25	10 to 20	50	30
Engine Silencing	Residential class mufflers	5 to 10	5 to 10	20	20
Substitution by alternative process	Use electric motors in preference to diesel or petrol	-	15 to 25	-	40

The Renzo Tonin & Associates' listed noise reductions are conservatively low and should be referred to in preference to those of AS2436.

Table 4.13 below identifies possible noise control measures, which are applicable on the construction plant likely to be used on site.

Table 4.13 – Noise Control Measures for Likely Construction Plant

Plant Description	Screening	Acoustic Enclosures	Silencing	Alternative Process
Small pile driving rig	✓	×	~	✓
Crane	✓	•	~	×
Drum roller	✓	×	~	×
Padfoot roller	✓	×	~	×
Wheeled loader	✓	×	~	×
Dump truck	✓	×	~	×

Plant Description	Screening	Acoustic Enclosures	Silencing	Alternative Process
30t Excavator	~	×	✓	×
Grader	~	×	~	×
Chain trencher	~	×	~	✓
Water truck	~	×	•	×
Telehandler	~	×	~	×
Forklift	~	×	✓	×

4.5.2 Noise Management Measures

In addition to physical noise controls, the following general noise management measures should be followed:

- Use less noisy plant and equipment, where feasible and reasonable.
- Plant and equipment should be properly maintained.
- Provide special attention to the use and maintenance of 'noise control' or 'silencing' kits fitted to machines to ensure they perform as intended.
- Strategically position plant on site to reduce the emission of noise to the surrounding neighbourhood and to site personnel.
- Avoid any unnecessary noise when carrying out manual operations and when operating plant.
- Any equipment not in use for extended periods during construction work should be switched off
- In addition to the noise mitigation measures outlined above, a management procedure
 would need to be put in place to deal with noise complaints that may arise from construction
 activities. Each complaint would need to be investigated and appropriate noise amelioration
 measures put in place to mitigate future occurrences, where the noise in question is in excess
 of allowable limits.
- Good relations with people living and working in the vicinity of a construction site should be
 established at the beginning of a project and be maintained throughout the project, as this is
 of paramount importance. Keeping people informed of progress and taking complaints
 seriously and dealing with them expeditiously is critical. The person selected to liaise with
 the community should be adequately trained and experienced in such matters.

Where noise level exceedances cannot be avoided, then consideration may be given to implementing time restrictions and/or providing periods of repose for residents, where feasible and reasonable. That is, daily periods of respite from noisy activities may also be scheduled for building occupants during construction hours.

Some items of plant may exceed noise limits even after noise treatment is applied. To reduce the overall noise impact, the use of noisy plant may be restricted to within certain time periods, where feasible and reasonable and to be negotiated with Council and the residents. Allowing the construction activities to proceed, despite the noise exceedance may be the preferred method in order to complete the works expeditiously.

5 Operational Noise Assessment

5.1 Operational Noise Criteria

Noise impact from the general operation of the proposed solar farm is assessed against the recently released NSW 'Noise Policy for Industry' (NPfI, 2017). The assessment procedure in terms of the NPfI has two components:

- Controlling intrusive noise impacts in the short-term for residences; and
- Maintaining noise level amenity for residences and other land uses.

In accordance with the NPfI, noise impact should be assessed against the project noise trigger level which is the lower value of the project intrusiveness noise levels and project amenity noise levels.

5.1.1 Intrusive Noise Impacts

According to the NPfl, the intrusiveness of a noise source may generally be considered acceptable if the equivalent continuous (energy-average) A-weighted level of noise from the source (represented by the L_{Aeq,15min} descriptor) does not exceed the background noise level measured in the absence of the source by more than 5dB(A). The project intrusiveness noise level, which is only applicable to residential receivers, is determined as follows:

L_{Aeq,15minute} Intrusiveness noise level = Rating Background Level (RBL) plus 5dB(A)

Based on the RBLs set in Table 3.2, the intrusiveness noise level for the residential receivers are determined in Table 5.1.

Table 5.1 - NPfl Intrusive Noise Level at Residential Receivers, dB(A)

Period	Rating Background Level, dB(A)	Intrusiveness Noise Level, L _{Aeq,15min} , dB(A)
Daytime	35	35+5 = 40
Evening	34	34+5 = 39
Night-time	30	30+5 = 35

5.1.2 Protecting Noise Amenity

The project amenity noise levels for different time periods of a day are determined in accordance with Section 2.4 of the NSW NPfl. The NPfl recommends amenity noise levels (L_{Aeq, period}) for various receivers including residential, commercial, industrial receivers and sensitive receivers such as schools, hotels, hospitals, churches and parks. These "recommended amenity noise levels" represent the objective for total industrial noise experienced at a receiver location. However, when assessing a single industrial development and its impact on an area, "project amenity noise levels" apply.

To ensure that the total industrial noise level (existing plus new) remain within the recommended amenity noise levels for an area, the project amenity noise level that applies for each new industrial noise source is determined as follows:

L_{Aeq,period} Project amenity noise level = L_{Aeq,period} Recommended amenity noise level - 5dB(A)

Furthermore, given that the intrusiveness noise level is based on a 15 minute assessment period and the project amenity noise level is based on day, evening and night assessment periods, the NPfl provides the following guidance on adjusting the $L_{Aeq,period}$ level to a representative $L_{Aeq,15minute}$ level in order to standardise the time periods.

$$L_{Aea.15min} = L_{Aea.period} + 3dB(A)$$

The policy, in accordance with the NPfI, applies an adjustment of (+3 dB) to the recommended noise levels ($L_{Aeq, period}$) in order to standardise the time periods for the intrusiveness and amenity noise levels. The project amenity noise levels ($L_{Aeq, 15min}$) applied for this project are reproduced in Table 5.2.

It is noted that the residential receivers in the vicinity of the site have been categorised as being in n 'rural' area in accordance with Table 2.3 of the NPfl.

Table 5.2 - NPfl Project Amenity Noise Levels, dB(A)

Type of Receiver	Indicative Noise Amenity Area	Time of Day		mended e Level
	Amenity Area		L _{Aeq} , Period	L _{Aeq} , 15min
Residence	Rural	Day	50 – 5 = 45	45 + 3 = 48
		Evening	45 - 5 = 40	40 + 3 = 43
		Night	40 - 5 = 35	35 + 3 = 38
Commercial Premises	All	When in use	65 – 5 = 60	60 + 3 = 63
Industrial Premises	All	When in use	70 – 5 = 65	65 + 3 = 68

Notes:

- 1. Monday-Saturday, Daytime 7.00 am to 6.00 pm; Evening 6.00 pm to 10.00 pm; Night-time 10.00 pm to 7.00 am.
- 2. On Sundays and Public Holidays, Daytime 8.00 am 6.00 pm; Evening 6.00 pm 10.00 pm; Night-time 10.00 pm 8.00 am.
- The L_{Aeq} index corresponds to the level of noise equivalent to the energy average of noise levels occurring over a measurement period.

5.2 Summary of Project Noise Trigger Levels

In accordance with the NPfl the project noise trigger level, which is the lower (ie. more stringent) value of the project intrusiveness noise level and project amenity noise level, has been determined and reproduced in Table 5.3 below.

Table 5.3 – Project Noise Trigger Levels, dB(A)

Receiver Location	L _{Aeq, 15min} Project Noise Trigger Levels				
Receiver Location	Day	Evening	Night		
Receiver R1 – 104 Cobbora Rd, Maryvale	40	39	35		
Receiver R2 – 215 Cobbora Rd, Maryvale	40	39	35		
Receiver R3 – 301 Cobbora Rd, Maryvale	40	39	35		
Receiver R4 – 66 Campbells Ln, Bodangora	40	39	35		
Receiver R5 – 6219 Goolma Rd Bodangora	40	39	35		
Receiver R6 – Lot 5 DP 664334 Gladstone Rd, Bodangora	40	39	35		
Receiver R7 – 104 Gladstone Road, Bodangora ⁴	68	68	68		
Receiver R8 – Wellington Correction Centre ⁴	63	63	63		
Receiver R9 – 28 Cadia Pl, Wuuluman	40	39	35		
Receiver R10 – 6582 Goolma Road, Bodangora – Soil Conservation Service ⁴	63	63	63		
Receiver R11 – 152 Bela Vista Ln, Montefiores	40	39	35		
Receiver R12 – 6938 Goolma Rd, Montefiores	40	39	35		
Receiver R13 – 7009 Goolma Rd, Montefiores	40	39	35		
Receiver R14 – 59 Twelve Mile Road, Wuuluman	40	39	35		
Receiver R15 – 6773 Goolma Road, Wuuluman	40	39	35		
Receiver R16 – 6916 Goolma Road, Wuuluman	40	39	35		

Notes: 1. Monday-Saturday, Daytime 7.00 am to 6.00 pm; Evening 6.00 pm to 10.00 pm; Night-time 10.00 pm to 7.00 am.

- 2. On Sundays and Public Holidays, Daytime 8.00 am 6.00 pm; Evening 6.00 pm 10.00 pm; Night-time 10.00 pm 8.00 am.
- 3. The L_{Aeq} index corresponds to the level of noise equivalent to the energy average of noise levels occurring over a measurement period.
- 4. Project Noise Trigger Levels only apply when premises are in use.

5.3 Operational Noise Sources

The proposed solar farm considers two options for the configuration of the PV panels:

- Fixed configuration, where the panels would be placed on fixed frames running in rows from West to west and tilted to the north; or
- 2. Single axis tracking, where the panels would be in rows configured in a north to south direction and the panels would track the sun from West to west throughout the day.

The single axis tracking system involves the panels being driven by motors to track the arc of the sun to maximise the solar effect. Hence, the tracking motors are a potential source of mechanical noise and therefore, has been included for a more conservative assessment. Up to a total of 13,367 tracking motors (NexTracker or equivalent) will be employed to drive the solar panels and are to be evenly distributed across the solar farm area. The tracking motors would turn no more than five (5) degrees every 15 minutes and would operate no more than one (1) minute out of every 15 minute period.

In addition to the trackers, the site will require the operation of up to 155 inverters (Ingeteam 1640TL B630) which will be evenly distributed across the solar farm area. A new substation will also be located near the southern end of the site. The dominant noise source from the new substation will be from two (2) 175MVA transformers. Furthermore, it is proposed that the existing substation located to the south of the project site and along Goolma Road may be upgraded with two (2) additional 175MVA transformers alongside the two (2) existing 375MVA transformers. The sound power level data for the existing 375MVA transformers were provided by the client and were measured to be 96dB(A) each. To provide a conservative assessment it was assumed that all the existing and proposed transformers have the same sound power level as the existing larger 375MVA transformer.

During operations, it is assumed that four (4) staff members will attend site daily during the day time period to inspect the equipment. It is also assumed that each staff member will travel around the subject site in a light vehicle.

Based on the above, the following table lists associated plant and equipment likely to be used for the operation of the proposed solar farm and their corresponding sound power levels.

Table 5.4 – Typical Operational Plant and Equipment & Sound Power Levels

Plant Item	Plant Description	L _{Aeq} Sound Power Levels, dB(A) re. 1pW
1	Tracker Motor (up to 13,367 in total)	78 (each)
2	Ingeteam 1640TL B630 Inverters (up to 155)	88 (each)
4	New 175MVA transformer (4 in total)	96 (each) ¹
5	Existing 375MVA transformers (2 in total)	96 (each) ¹
6	Light vehicle (4 in total)	88 (each)

Notes: 1. Based on sound power level data provided by the client

The sound power levels for the plant and equipment presented in the above table are provided by the manufacturer, information from past projects and/or information held in our library files.

5.4 'Modifying Factor' Adjustments

Further to the above and in accordance with the NPfl, where the character of the noise in question is assessed as particularly annoying (ie. if it has an inherently tonal, low frequency, impulsive or intermittent characteristic), then an adjustment of 5dB(A) for each annoyance aspect, up to a total of 10dB(A), is to be added to the predicted value to penalise the noise for its potential increase in annoyance.

Table C1 in Fact Sheet C of the NSW NPfl provides definitive procedures for determining whether a penalty or adjustment should be applied from increased annoyance. For the assessment of the solar farm, the noise from the inverters and transformers are considered to be tonal in nature. Therefore, a 5dB(A) penalty has been applied to the predicted noise contributions from the inverters and transformers.

5.5 Operational Noise Assessment

Noise emissions were predicted by modelling the noise sources, receiver locations, topographical features of the intervening area, and possible noise control treatments using CadnaA (version 2018) noise modelling computer program. The program calculates the contribution of each noise source at each specified receptor point and allows for the prediction of the total noise from a site.

The noise prediction models takes into account:

- Location of noise sources and receiver locations;
- Height of sources and receivers;
- Separation distances between sources and receivers;
- Ground type between sources and receivers (soft); and
- Attenuation from barriers (natural and purpose built).

Furthermore, in accordance with the NPfI noise predictions were prepared for each of the following meteorological conditions:

- 1. Calm & isothermal conditions (acoustically neutral) no wind and no temperature inversion
- 2. Slight to gentle breeze 3m/s wind velocity at 10m from ground level between each noise source and each noise receiver (as per NPfl default wind conditions). Wind direction was based on wind travelling from the source to the receiver.
- 3. Moderate temperature inversion applicable for noise predictions during night time periods only

Table 5.5 below present the predicted noise levels for the worst case scenario based on concurrent operation of all the plant and equipment shown in Table 5.4. The tracker motors were time corrected based on their operation of one (1) minute out of a 15 minute period.

10 AUGUST 2018 RENZO TONIN & ASSOCIATES

Table 5.5 – Predicted L_{Aeq,15min} Operational Noise Levels at Receiver Locations, dB(A)

	Project Noise Trigger Levels ¹		Predicted Operational Noise Levels, L _{Aeq, 15min}										
Receiver Location			Calm & Isothermal Conditions			Slight to Gentle Breeze			Moderate Temperature Inversion ²			Comply?	
	Day	Evening	Night	Solar Plant	Upgraded Substation	Cumulative ⁴	Solar Plant	Upgraded Substation	Cumulative ⁴	Solar Plant	Upgraded Substation	Cumulative ⁴	(Yes/No)
Receiver R1	40	39	35	24	<20	24	30	22	31	30	22	30	Yes
Receiver R2	40	39	35	30	<20	30	34	<20	34	34	<20	34	Yes
Receiver R3	40	39	35	28	<20	28	33	<20	33	33	<20	33	Yes
Receiver R4	40	39	35	28	<20	28	32	<20	32	33	<20	33	Yes
Receiver R5	40	39	35	<20	<20	<20	26	<20	26	26	<20	26	Yes
Receiver R6	40	39	35	28	<20	28	33	<20	33	33	<20	33	Yes
Receiver R7 ³	68	68	68	26	<20	26	32	<20	32	32	<20	32	Yes
Receiver R8 ³	63	63	63	25	<20	26	31	24	32	31	24	31	Yes
Receiver R9	40	39	35	<20	23	24	26	29	31	26	29	31	Yes
Receiver R10 ³	63	63	63	31	<20	31	34	25	35	35	25	35	Yes
Receiver R11	40	39	35	<20	<20	21	26	24	28	26	24	28	Yes
Receiver R12	40	39	35	<20	24	25	25	30	31	25	30	31	Yes
Receiver R13	40	39	35	<20	27	27	22	33	33	22	33	33	Yes
Receiver R14	40	39	35	<20	28	28	25	33	34	25	33	34	Yes
Receiver R15	40	39	35	<20	28	28	21	33	33	21	33	33	Yes
Receiver R16	40	39	35	27	22	28	33	28	34	33	28	34	Yes

- Notes: 1. Trigger levels for Day, Evening and Night periods
 - 2. Applicable for the night time period only
 - 3. When in use
 - 4. Overall noise contribution from solar plant and the upgraded substation

Based on the predicted noise levels presented in the table above, operational noise levels from the proposed solar farm and the upgraded substation at the nearest receivers each comply with the nominated project trigger levels under all scenarios and meteorological conditions. Furthermore, the predicted cumulative noise levels from the operation of the solar farm and the upgraded substation comply with the project trigger levels for each receiver under all scenarios and meteorological conditions.

Therefore, no further reasonable and feasible noise mitigation measures are required to reduce operational noise impacts.

5.6 Cumulative Operation Noise Assessment

It is likely that the Wellington South Solar Plant would be operating concurrently with the Wellington North Solar Plant. Therefore, cumulative noise impacts at the nearest affected receivers due to both solar plants operating has been considered. The predicted operation noise from the South Solar Plant has been detailed in the noise and vibration assessment of the Wellington Solar Plant [ref: TJ643-01F01 Report (r5), dated 24 November 2017].

An assessment of cumulative noise impacts from the Wellington North Solar Plant, the upgraded substation and the Wellington Solar Plant has been quantified only for the nearest affected receivers potentially impacted by cumulative noise from both solar plants and the upgraded substation. The cumulative noise levels are presented in Table 5.6 for the applicable meteorological conditions.

Table 5.6 – Predicted L_{Aeq,15min} Cumulative Operational Noise Levels at Receiver Locations, dB(A)

	Proje	ct Noise Tr	igger	Predicted Operational Noise Levels, L _{Aeq, 15min}												
Levels Receiver		Calm & Isothermal Conditions				Slight to Gentle Breeze			Moderate Temperature Inversion ¹				Comply?			
Location	Day	Evening	Night	North Solar Plant	Upgraded Substation	South Solar Plant	Cumulative ³	North Solar Plant	Upgraded Substation	South Solar Plant	Cumulative ³	North Solar Plant	Upgraded Substation	South Solar Plant	Cumulative ³	(Yes/No)
Receiver R1	40	39	35	24	<20	25	28	30	22	30	33	30	22	30	33	Yes
Receiver R2	40	39	35	30	<20	<20	30	34	<20	25	35	34	<20	25	35	Yes
Receiver R8 ²	63	63	63	25	<20	26	29	31	24	32	35	31	24	32	35	Yes
Receiver R9	40	39	35	<20	23	27	29	26	29	31	34	26	29	31	34	Yes
Receiver R10 ²	63	63	63	31	<20	28	33	34	25	33	37	35	25	33	37	Yes
Receiver R11	40	39	35	<20	<20	22	25	26	24	28	31	26	24	28	31	Yes
Receiver R12	40	39	35	<20	24	25	28	25	30	31	34	25	30	31	34	Yes
Receiver R13	40	39	35	<20	27	22	28	22	33	28	34	22	33	28	34	Yes
Receiver R14	40	39	35	<20	28	31	33	25	33	35	37	25	33	35	37	No

Notes: 1. Applicable for the night time period only

^{2.} Commercial receiver assessed only for when in use

^{3.} Overall noise contribution from Wellington North Solar Plant, upgraded substation and Wellington Solar Plant

^{4.} **Bold** font indicates exceedance

From Table 5.6 it can be seen that the predicted noise levels generally comply at all receiver locations under all scenarios and meteorological conditions. However, under noise enhancing weather conditions, the predicted cumulative noise levels at Receiver R14 exceed the criterion by 2dB(A) during the night period. The exceedance at R14 is mainly attributed to the noise emissions from the South Solar Farm, which predicts noise levels equal to the night time Project Noise Trigger Level of 35dB(A). When the noise emissions from the upgraded substation is considered, it is predicted to increase the overall noise levels by 2dB(A) at the receiver and therefore yielding an exceedance of 2dB(A) at Receiver R14.

In accordance with Table 4.1 and Table 4.2 of the NPfl, a 2dB(A) exceedance is considered to be negligible as a 2dB(A) change in noise level is not discernible or noticeable to the average person. Therefore, the predicted noise levels at Receiver R14 are determined to be acceptable in accordance with the NPfl and no further reasonable and feasible noise mitigation measures are required.

5.7 Sleep Disturbance Assessment

To assess the likelihood of sleep disturbance, the potential of maximum noise level events from premises during the night-time period has been considered in this assessment. In accordance with NPfl, a detailed maximum noise level event assessment should be undertaken where the subject development night-time noise levels at a residential location exceed:

- L_{Aeq.15min} 40dB(A) or the prevailing RBL plus 5dB, whichever is the greater, and/or
- LAFmax 52dB(A) or the prevailing RBL plus 15dB, whichever is the greater.

Where there are noise events found to exceed the initial screening level, further analysis is undertaken to identify:

- The likely number of events that might occur during the night assessment period,
- The extent to which the maximum noise level exceeds the rating background noise level.

During the night time period, only mechanical plant will be operating, including the tracking motors, inverters and the substations. Noise emissions from these plant items are considered to be continuous with no potential for high peak noise level events. Therefore, the L_{Amax} noise levels experienced at the identified receivers will be similar to the predicted $L_{Aeq,15min}$ noise levels shown in Table 5.5. Hence, it is expected that both the $L_{Aeq,15min}$ and L_{AFmax} will be well below the nominated sleep disturbance criteria of 40dB(A) and 52dB(A), respectively.

6 Vibration Assessment

Vibration generating activities would occur only during the construction phase of the project. There are no vibration generating activities expected during the operational phase. As the nearest identified receivers are in excess of 50m from the subject site, structural damage due to vibration is not expected. Assessment for vibration impact on human comfort is assessed in accordance with EPA requirements.

6.1 Vibration Criteria

Assessment of potential disturbance from vibration on human occupants of buildings is made in accordance with the EPA's 'Assessing Vibration; a technical guideline' (DECC, 2006). The guideline provides criteria which are based on British Standard BS 6472-1992 'Evaluation of human exposure to vibration in buildings (1-80Hz)'. Sources of vibration are defined as either 'Continuous', 'Impulsive' or 'Intermittent'. Table 6.1 provides definitions and examples of each type of vibration.

Table 6.1 – Types of Vibration

Type of Vibration	Definition	Examples
Continuous vibration	Continues uninterrupted for a defined period (usually throughout the day-time and/or night-time)	Machinery, steady road traffic, continuous construction activity (such as tunnel boring machinery).
Impulsive vibration	A rapid build-up to a peak followed by a damped decay that may or may not involve several cycles of vibration (depending on frequency and damping). It can also consist of a sudden application of several cycles at approximately the same amplitude, providing that the duration is short, typically less than 2 seconds	Infrequent: Activities that create up to 3 distinct vibration events in an assessment period, e.g. occasional dropping of heavy equipment, occasional loading and unloading.
Intermittent vibration	Can be defined as interrupted periods of continuous or repeated periods of impulsive vibration that varies significantly in magnitude	Trains, nearby intermittent construction activity, passing heavy vehicles, forging machines, impact pile driving, jack hammers. Where the number of vibration events in an assessment period is three or fewer, this would be assessed against impulsive vibration

Source: Assessing Vibration; a technical guideline, Department of Environment & Climate Change, 2006

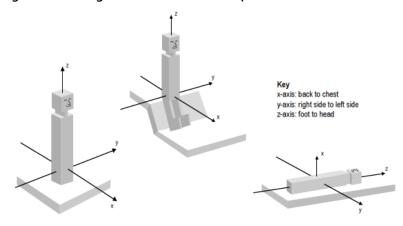
The vibration criteria are defined as a single weighted root mean square (rms) acceleration source level in each orthogonal axis. Section 2.3 of the guideline states:

"Evidence from research suggests that there are summation effects for vibrations at different frequencies. Therefore, for evaluation of vibration in relation to annoyance and comfort, overall weighted rms acceleration values of the vibration in each orthogonal axis are preferred (BS 6472)."

When applying the criteria, it is important to note that the three directional axes are referenced to the human body, i.e. x-axis (back to chest), y-axis (right side to left side) or z-axis (foot to head). Vibration may enter the body along different orthogonal axes and affect it in different ways. Therefore, application of the criteria requires consideration of the position of the people being assessed, as

illustrated in Figure 2. For example, vibration measured in the horizontal plane is compared with x- and y-axis criteria if the concern is for people in an upright position, or with the y- and z- axis criteria if the concern is for people in the lateral position.

Figure 2 – Orthogonal Axes for Human Exposure to Vibration



The preferred and maximum values for continuous and impulsive vibration are defined in Table 2.2 of the guideline and are reproduced in Table 6.2 for the applicable receivers.

Table 6.2 - Preferred and Maximum Levels for Human Comfort

14:	A	Prefer	red Values	Maximum Values		
Location	Assessment Period ¹	z-axis	x- and y-axis	z-axis	x- and y-axis	
Continuous vibration (weighted RI	MS acceleration, m/s ² , 1-	80Hz)				
Residences	Daytime	0.010	0.0071	0.020	0.014	
	Night-time	0.007	0.005	0.014	0.010	
offices, schools, educational Day or night-time		0.020	0.014	0.040	0.028	
Impulsive vibration (weighted RMS	S acceleration, m/s², 1-80	Hz)				
Residences	Daytime	0.30	0.21	0.60	0.42	
	Night-time	0.10	0.071	0.20	0.14	
Offices, schools, educational institutions and places of worship	Day or night-time	0.64	0.46	1.28	0.92	

Notes: 1. Daytime is 7:00am to 10:00pm and Night-time is 10:00pm to 7:00am

The acceptable vibration dose values (VDV) for intermittent vibration are defined in Table 2.4 of the guideline and are reproduced in Table 6.3 for the applicable receiver type.

Table 6.3 – Acceptable Vibration Dose Values for Intermittent Vibration (m/s^{1.75})

Location	Day	time ¹	Night-time ¹		
Location	Preferred Value	Maximum Value	Preferred Value	Maximum Value	
Residences	0.20	0.40	0.13	0.26	
Offices, schools, educational institutions and places of worship	0.40	0.80	0.40	0.80	

Notes: 1. Daytime is 7:00am to 10:00pm and Night-time is 10:00pm to 7:00am

6.2 Potential Vibration Impacts

Based on the proposed plant items presented in Table 4.4, vibration generated by construction plant was estimated and potential vibration impacts are summarised in Table 6.4 below. The assessment is relevant to the identified receiver locations.

Table 6.4 - Potential Vibration Impacts for Identified Receivers

Approx. Distance to Nearest Buildings from Works	Type of Nearest Sensitive Buildings	Assessment on Potential Vibration Impacts	Vibration Monitoring
330m	Residential	Very low risk of adverse comments	Not required
135m	Residential	Very low risk of adverse comments	Not required
315m	Residential	Very low risk of adverse comments	Not required
110m	Residential	Very low risk of adverse comments	Not required
910m	Residential	Very low risk of adverse comments	Not required
225m	Residential	Very low risk of adverse comments	Not required
330m	Commercial	Very low risk of adverse comments	Not required
400m	Commercial	Very low risk of adverse comments	Not required
1220m	Residential	Very low risk of adverse comments	Not required
75m	Commercial	Very low risk of adverse comments	Not required
580m	Residential	Very low risk of adverse comments	Not required
250m	Residential	Very low risk of adverse comments	Not required
530m	Residential	Very low risk of adverse comments	Not required
350m	Residential	Very low risk of adverse comments	Not required
	Nearest Buildings from Works 330m 135m 315m 110m 910m 225m 330m 400m 1220m 75m 580m 250m 530m	Nearest Buildings from Works 330m Residential 135m Residential 315m Residential 110m Residential 910m Residential 225m Residential 400m Commercial 1220m Residential 75m Commercial 580m Residential 250m Residential Residential	Nearest Buildings from Works Type of Nearest Sensitive Buildings Assessment on Potential Vibration Impacts 330m Residential Very low risk of adverse comments 135m Residential Very low risk of adverse comments 315m Residential Very low risk of adverse comments 110m Residential Very low risk of adverse comments 910m Residential Very low risk of adverse comments 225m Residential Very low risk of adverse comments 330m Commercial Very low risk of adverse comments 400m Commercial Very low risk of adverse comments 1220m Residential Very low risk of adverse comments 580m Residential Very low risk of adverse comments 250m Residential Very low risk of adverse comments 530m Residential Very low risk of adverse comments

Receiver Location	Approx. Distance to Nearest Buildings from Works	Type of Nearest Sensitive Buildings	Assessment on Potential Vibration Impacts	Vibration Monitoring
Receiver R15	1300m	Residential	Very low risk of adverse comments	Not required
Receiver R16	760m	Residential	Very low risk of adverse comments	Not required

The potential for adverse comments to vibration impacts during the construction works was determined to be very low due to the large distances between the receiver locations and the construction activities. Therefore, additional vibration mitigation measures and vibration monitoring are not required at the identified receiver locations during construction works associated with the project.

7 Road Traffic Noise Assessment

Noise impact from the potential increase in traffic on the surrounding road network due to construction and operational activities is assessed against the NSW 'Road Noise Policy' (RNP, 2011). The RNP sets out criteria to be applied to particular types of road and land uses. These noise criteria are to be applied when assessing noise impact and determining mitigation measures for sensitive receivers that are potentially affected by road traffic noise associated with the construction and operation of the subject site, with the aim of preserving the amenity appropriate to the land use.

Vehicle access to the subject site will be via Campbells Lane. Based on information provided by the client, the maximum trips per day throughout the construction stage are presented in Table 7.1. The trips per day were multiplied by a factor of two (2) in the noise prediction model, as it assumes that each single trip will enter and exit through Campbells Lane. Furthermore, vehicle movements will only occur during the day time period when construction works occur. Therefore, to determine the average hourly vehicle movements to and from the site, the daily vehicle movements were divided by 11 to represent the weekday construction hours from 7am to 6pm.

Table 7.1 – Summary of the Estimated Construction Traffic Volumes During Peak Construction

Vehicle Type	Trips per Day	Movements per Day ¹	Average Hourly Movements ²
Cars/ light vehicles	17	34	3
Trucks/ heavy vehicles	52	104	10

Notes: 1. Movements per day based on 2 x trips per day, representing vehicles entering and exiting the site

During the operational stage, vehicle access to the site will be maintenance vans and delivery trucks (4 \times site staff light vehicle and 5 \times miscellaneous courier deliveries per week) which would occur on an irregular basis. Therefore, traffic noise impacts during the operational stage of the project would be minimal and insignificant and will not be assessed further.

7.1 Road Traffic Noise Criteria

Based on functionality, Campbells Lane is categorised as a local road. For existing residences affected by additional traffic on existing local roads generated by land use developments, the following RNP road traffic noise criteria apply.

Table 7.2 - RNP Road Traffic Noise Criteria, dB(A)

		Assessment C	Assessment Criteria, dB(A)	
Road Category	Type of Project/Land Use	Day 7am – 10pm	Night 10pm – 7am	
Local road	6. Existing residences affected by additional traffic on existing local roads generated by land use developments	L _{Aeq,(1 hour)} 55 (external)	L _{Aeq,(1 hour)} 50 (external)	

^{2.} Average hourly movements based on movements per day ÷ 11, representing construction hours from 7am to 6pm

A traffic survey to determine existing traffic volumes along Campbells Lane was undertaken by GHD and detailed in the 'Traffic and Parking Assessment' (ref 4131379, dated May 2018). The existing traffic volumes recorded are reproduced in the table below.

Table 7.3 – Exiting Traffic Volumes Along Campbells Lane

Campbells Lane	Average Weekday AM Peak Hour ¹	Average Weekday PM Peak Hour ¹	Saturday Peak Hour ¹	Weekday Heavy Vehicle %	Weekend Heavy Vehicles %	Speed Limit ²
Westbound	2	3	1	120/	70/	100
Westbound	2	5	4	12%	7%	km/h

Notes: 1. Vehicles per hour

7.2 Predicted Road Traffic Noise

From Table 7.3, the existing worst case hourly traffic volumes along Campbells Lane occur during the weekday PM peak hour period. Furthermore, the average hourly vehicle movements presented in Table 7.1 were used to represent the additional traffic along Campbells Lane during construction of the project. Results of the road traffic noise predictions are presented in the table below.

Table 7.4 - Predicted Road Traffic Noise Contribution Levels Along Public Roads, dB(A) LAeq(1 Hour)

		Traffic Movements		Speed	Approx.	Predicted	
Receiver	Criteria	Light Heavy Vehicle Vehicle		(km/h)	Distance to Road	Noise Level	Exceed?
Nearest receivers	L _{Aeq, (1 hour)} 55	11 (8 + 3)	11 (1 + 10)	100	110m	55	No

From the above table, traffic noise levels along Campbells Lane due to additional traffic during the construction stage of the project is predicted to comply with applicable noise criterion at the nearest affected receivers.

As the construction traffic noise levels are temporary and comply with the RNP criteria set above, it indicates that the traffic noise levels due to the construction works for the solar farm would not adversely affect the existing residences along Campbells Lane.

^{2.} Speed limit provided in Table 2-3 of the 'Traffic and Parking Assessment' prepared by GHD

8 Conclusion

Renzo Tonin and Associates has completed an environmental noise and vibration assessment of the proposed Wellington North Solar Plant.

Noise emissions from the construction phase of the project were predicted to exceed the construction noise management levels at the nearest affected receivers. In-principle recommendations are provided in Section 4.5 to limit the potential impact of noise generated by construction activities to acceptable levels.

Noise emissions from the operational phase of the project were predicted to comply with the nominated criteria at the nearest affected receivers.

Given the large separation distance between the nearest affected receivers and the subject site, vibration impacts resulting in structural damage to buildings at the nearest affected receivers are determined to be negligible and there is low risk of adverse comments from occupants of dwellings due to construction vibration.

Road traffic noise impacts on residential properties along the access route were found to comply with the relevant RNP criteria.

APPENDIX A Glossary of Terminology

The following is a brief description of the technical terms used to describe noise to assist in understanding the technical issues presented.

Adverse weather	Weather effects that enhance noise (that is, wind and temperature inversions) that occur at a site for a significant period of time (that is, wind occurring more than 30% of the time in any assessment period in any season and/or temperature inversions occurring more than 30% of the nights in winter).
Ambient noise	The all-encompassing noise associated within a given environment at a given time, usually composed of sound from all sources near and far.
Assessment period	The period in a day over which assessments are made.
Assessment point	A point at which noise measurements are taken or estimated. A point at which noise measurements are taken or estimated.
Background noise	Background noise is the term used to describe the underlying level of noise present in the ambient noise, measured in the absence of the noise under investigation, when extraneous noise is removed. It is described as the average of the minimum noise levels measured on a sound level meter and is measured statistically as the A-weighted noise level exceeded for ninety percent of a sample period. This is represented as the L90 noise level (see below).
Decibel [dB]	The units that sound is measured in. The following are examples of the decibel readings of every day sounds: OdB The faintest sound we can hear 30dB A quiet library or in a quiet location in the country 45dB Typical office space. Ambience in the city at night 60dB CBD mall at lunch time 70dB The sound of a car passing on the street 80dB Loud music played at home 90dB The sound of a truck passing on the street 100dBThe sound of a rock band 110dBOperating a chainsaw or jackhammer 120dBDeafening
dB(A)	A-weighted decibels. The A- weighting noise filter simulates the response of the human ear at relatively low levels, where the ear is not as effective in hearing low frequency sounds as it is in hearing high frequency sounds. That is, low frequency sounds of the same dB level are not heard as loud as high frequency sounds. The sound level meter replicates the human response of the ear by using an electronic filter which is called the "A" filter. A sound level measured with this filter switched on is denoted as dB(A). Practically all noise is measured using the A filter.
dB(C)	C-weighted decibels. The C-weighting noise filter simulates the response of the human ear at relatively high levels, where the human ear is nearly equally effective at hearing from mid-low frequency (63Hz) to mid-high frequency (4kHz), but is less effective outside these frequencies.
Frequency	Frequency is synonymous to pitch. Sounds have a pitch which is peculiar to the nature of the sound generator. For example, the sound of a tiny bell has a high pitch and the sound of a bass drum has a low pitch. Frequency or pitch can be measured on a scale in units of Hertz or Hz.
Impulsive noise	Having a high peak of short duration or a sequence of such peaks. A sequence of impulses in rapid succession is termed repetitive impulsive noise.
Intermittent noise	The level suddenly drops to that of the background noise several times during the period of observation. The time during which the noise remains at levels different from that of the ambient is one second or more.
L _{Max}	The maximum sound pressure level measured over a given period.
L _{Min}	The minimum sound pressure level measured over a given period.

L ₁	The sound pressure level that is exceeded for 1% of the time for which the given sound is measured.
L ₁₀	The sound pressure level that is exceeded for 10% of the time for which the given sound is measured.
L ₉₀	The level of noise exceeded for 90% of the time. The bottom 10% of the sample is the L90 noise level expressed in units of dB(A).
L _{eq}	The "equivalent noise level" is the summation of noise events and integrated over a selected period of time.
Reflection	Sound wave changed in direction of propagation due to a solid object obscuring its path.
SEL	Sound Exposure Level (SEL) is the constant sound level which, if maintained for a period of 1 second would have the same acoustic energy as the measured noise event. SEL noise measurements are useful as they can be converted to obtain Leq sound levels over any period of time and can be used for predicting noise at various locations.
Sound	A fluctuation of air pressure which is propagated as a wave through air.
Sound absorption	The ability of a material to absorb sound energy through its conversion into thermal energy.
Sound level meter	An instrument consisting of a microphone, amplifier and indicating device, having a declared performance and designed to measure sound pressure levels.
Sound pressure level	The level of noise, usually expressed in decibels, as measured by a standard sound level meter with a microphone.
Sound power level	Ten times the logarithm to the base 10 of the ratio of the sound power of the source to the reference sound power.
Tonal noise	Containing a prominent frequency and characterised by a definite pitch.

APPENDIX B Long-Term Noise Monitoring Methodology

B.1 Noise Monitoring Equipment

A long-term unattended noise monitor consists of a sound level meter housed inside a weather resistant enclosure. Noise levels are monitored continuously with statistical data stored in memory for every 15-minute period.

Long term noise monitoring was conducted using the following instrumentation:

Description	Туре	Octave Band Data	Logger Location(s)
RTA04 (CESVA SC310)	Type 1	1/1	L1

Notes:

All meters comply with AS IEC 61672.1 2004 "Electroacoustics - Sound Level Meters" and designated either Type 1 or Type 2 as per table, and are suitable for field use.

The equipment was calibrated prior and subsequent to the measurement period using a Bruel & Kjaer Type 4231 calibrator. No significant drift in calibration was observed.

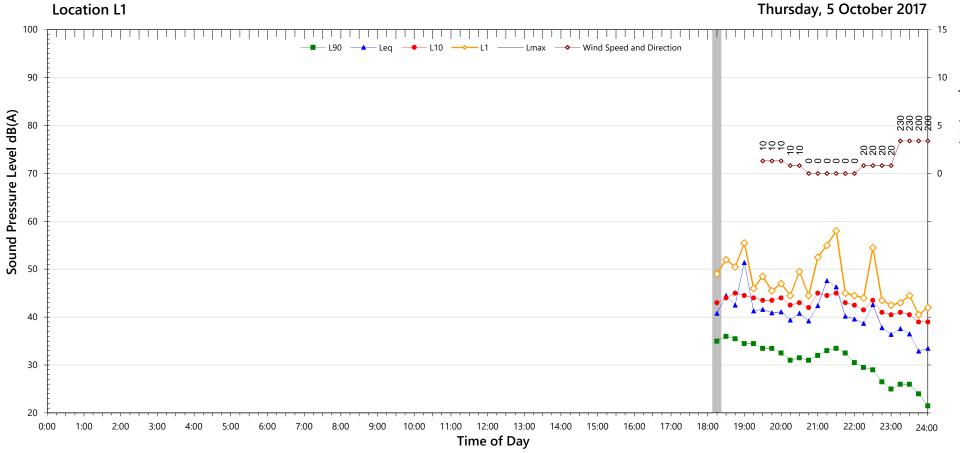
B.2 Meteorology During Monitoring

Measurements affected by extraneous noise, wind (greater than 5m/s) or rain were excluded from the recorded data in accordance with the NSW NPfl. Determination of extraneous meteorological conditions was based on data provided by the Bureau of Meteorology (BOM), for a location considered representative of the noise monitoring location(s). However, the data was adjusted to account for the height difference between the BOM weather station, where wind speed and direction is recorded at a height of 10m above ground level, and the microphone location, which is typically 1.5m above ground level (and less than 3m). The correction factor applied to the data is based on Table C.1 of ISO 4354:2009 'Wind actions on structures'.

B.3 Noise vs Time Graphs

Noise almost always varies with time. Noise environments can be described using various descriptors to show how a noise ranges about a level. In this report, noise values measured or referred to include the L_{10} , L_{90} , and L_{eq} levels. The statistical descriptors L_{10} and L_{90} measure the noise level exceeded for 10% and 90% of the sample measurement time. The L_{eq} level is the equivalent continuous noise level or the level averaged on an equal energy basis. Measurement sample periods are usually ten to fifteen minutes. The Noise -vs- Time graphs representing measured noise levels, as presented in this report, illustrate these concepts for the broadband dB(A) results.

APPENDIX C Long Term Noise Monitoring Results



NSW Industrial Noise Policy (Free Field)					
Descriptor	Day ²	Evening ³	Night ⁴⁵		
L ₉₀	-	31.0	18.5		
LAeq	-	44.3	45.0		

Night Time Maximum Noise Levels (see note 7)				
L _{Max} (Range)	-	to	-	
L _{Max} - L _{eq} (Range)	-	to	-	

NSW Road Noise Policy (1n	(see note 6)	
Descriptor	Day	Night⁵
Descriptor	7am-10pm	10pm-7am
L _{eq 15 hr} and L _{eq 9 hr}	46.8	47.5
L _{eq 1hr} upper 10 percentile	50.4	53.6
L _{ea 1hr} lower 10 percentile	43.1	28.9

^{1.} Shaded periods denote measurements adversely affected by rain, wind or extraneous noise - data in these periods are excluded from calculations.

^{2. &}quot;Day" is the period from 8am till 6pm on Sundays and 7am til 6pm on other days

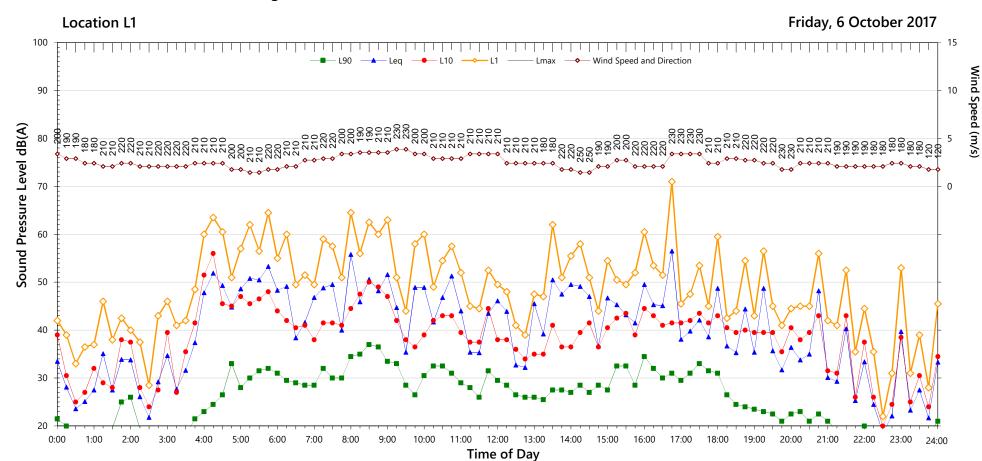
^{3. &}quot;Evening" is the period from 6pm till 10pm

^{4. &}quot;Night" relates to the remaining periods

^{5. &}quot;Night" relates to period from 10pm on this graph to morning on the following graph.

^{6.} Graphed data measured in free-field; tabulated results facade corrected

^{7.} Night time L_{Max} values are shown only where $L_{Max} > 65 dB(A)$ and where L_{Max} - Leq $\geq 15 dB(A)$



NSW Industrial Noise Policy (Free Field)				
Descriptor	Day ²	Evening ³	Night ^{4 5}	
L ₉₀	26.5	19.0	18.0	
LAeq	47.9	41.2	47.6	

Night Time Maximum Noise Levels (see note 7)			
L _{Max} (Range)	-	to	-
L _{Max} - L _{eq} (Range)	-	to	-

NSW Road Noise Policy (1n	(see note 6)	
Descriptor	Day	Night⁵
Descriptor	7am-10pm	10pm-7am
L _{eq 15 hr} and L _{eq 9 hr}	49.4	50.1
L _{eq 1hr} upper 10 percentile	53.8	55.1
L _{ea 1hr} lower 10 percentile	40.7	30.5

Notes:

^{1.} Shaded periods denote measurements adversely affected by rain, wind or extraneous noise - data in these periods are excluded from calculations.

^{2. &}quot;Day" is the period from 8am till 6pm on Sundays and 7am til 6pm on other days

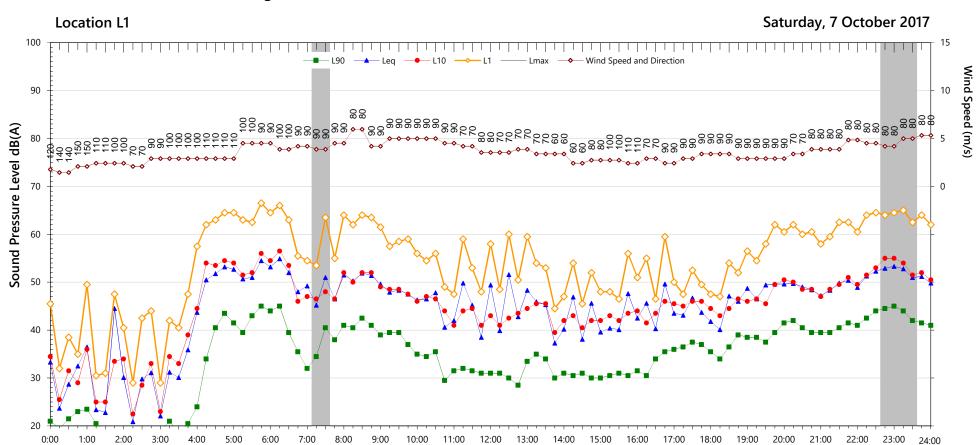
^{3. &}quot;Evening" is the period from 6pm till 10pm

^{4. &}quot;Night" relates to the remaining periods

^{5. &}quot;Night" relates to period from 10pm on this graph to morning on the following graph.

^{6.} Graphed data measured in free-field; tabulated results facade corrected

^{7.} Night time L_{Max} values are shown only where $L_{Max} > 65 dB(A)$ and where L_{Max} - Leq $\geq 15 dB(A)$



Time of Day

NSW Industrial Noise Policy (Free Field)				
Descriptor	Day ²	Evening ³	Night ^{4 5}	
L ₉₀	30.0	36.5	25.5	
LAeq	46.9	48.5	49.1	

5:00

Night Time Maximum Noise Levels (see note 7)			
L _{Max} (Range)	-	to	-
L _{Max} - L _{eq} (Range)	-	to	-

NSW Road Noise Policy (1n	(see note 6)	
Descriptor	Day	Night⁵
Descriptor	7am-10pm	10pm-7am
L _{eq 15 hr} and L _{eq 9 hr}	49.9	51.8
L _{eq 1hr} upper 10 percentile	52.8	55.7
L _{ea 1hr} lower 10 percentile	46.1	37.6

16:00

17:00

18:00

19:00

Notes:

0:00

^{1.} Shaded periods denote measurements adversely affected by rain, wind or extraneous noise - data in these periods are excluded from calculations.

^{2. &}quot;Day" is the period from 8am till 6pm on Sundays and 7am til 6pm on other days

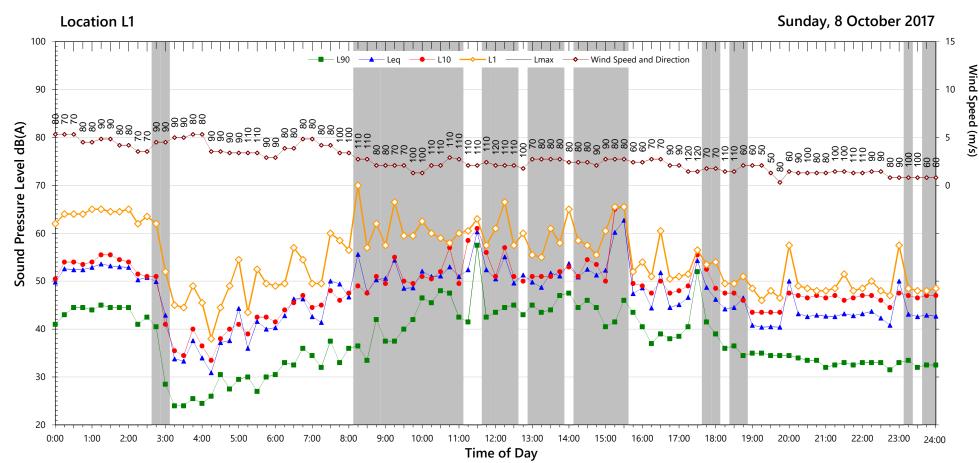
^{3. &}quot;Evening" is the period from 6pm till 10pm

^{4. &}quot;Night" relates to the remaining periods

^{5. &}quot;Night" relates to period from 10pm on this graph to morning on the following graph.

^{6.} Graphed data measured in free-field; tabulated results facade corrected

^{7.} Night time L_{Max} values are shown only where $L_{Max} > 65 dB(A)$ and where $L_{Max}^- Leq \ge 15 dB(A)$



NSW Industrial Noise Policy (Free Field)				
Descriptor	Day ²	Evening ³	Night ^{4 5}	
L ₉₀	38.0	32.5	29.0	
LAeq	52.8	43.7	48.4	

Night Time Maximum Noise Levels			(see note 7)
L _{Max} (Range)	-	to	-
L _{Max} - L _{eq} (Range)	-	to	-

NSW Road Noise Policy (1m	(see note 6)	
Day		Night⁵
Descriptor	7am-10pm	10pm-7am
L _{eq 15 hr} and L _{eq 9 hr}	52.3	50.9
L _{eq 1hr} upper 10 percentile	60.2	55.2
L _{eq 1br} lower 10 percentile	45.3	45.0

Notes:

^{1.} Shaded periods denote measurements adversely affected by rain, wind or extraneous noise - data in these periods are excluded from calculations.

^{2. &}quot;Day" is the period from 8am till 6pm on Sundays and 7am til 6pm on other days

^{3. &}quot;Evening" is the period from 6pm till 10pm

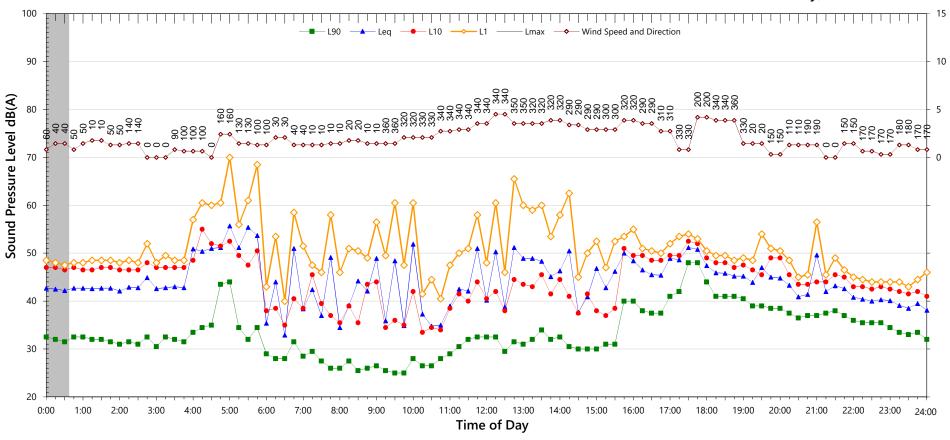
^{4. &}quot;Night" relates to the remaining periods

^{5. &}quot;Night" relates to period from 10pm on this graph to morning on the following graph.

^{6.} Graphed data measured in free-field; tabulated results facade corrected

^{7.} Night time L_{Max} values are shown only where $L_{Max} > 65 dB(A)$ and where L_{Max} - Leq $\geq 15 dB(A)$

Location L1 Monday, 9 October 2017



NSW Industrial Noise Policy (Free Field)				
Descriptor	Day ²	Evening ³	Night ^{4 5}	
L ₉₀	26.0	36.5	23.5	
LAeq	47.0	44.8	45.2	

Night Time Maximum Noise Levels			(see note 7)
L _{Max} (Range)	-	to	-
L _{Max} - L _{eq} (Range)	-	to	-

NSW Road Noise Policy (1m	(see note 6)	
Descriptor	Day	Night⁵
	7am-10pm	10pm-7am
L _{eq 15 hr} and L _{eq 9 hr}	49.0	47.7
L _{eq 1hr} upper 10 percentile	51.9	52.5
L _{eq 1hr} lower 10 percentile	42.8	36.3

Notes:

Wind Speed (m/s)

^{1.} Shaded periods denote measurements adversely affected by rain, wind or extraneous noise - data in these periods are excluded from calculations.

^{2. &}quot;Day" is the period from 8am till 6pm on Sundays and 7am til 6pm on other days

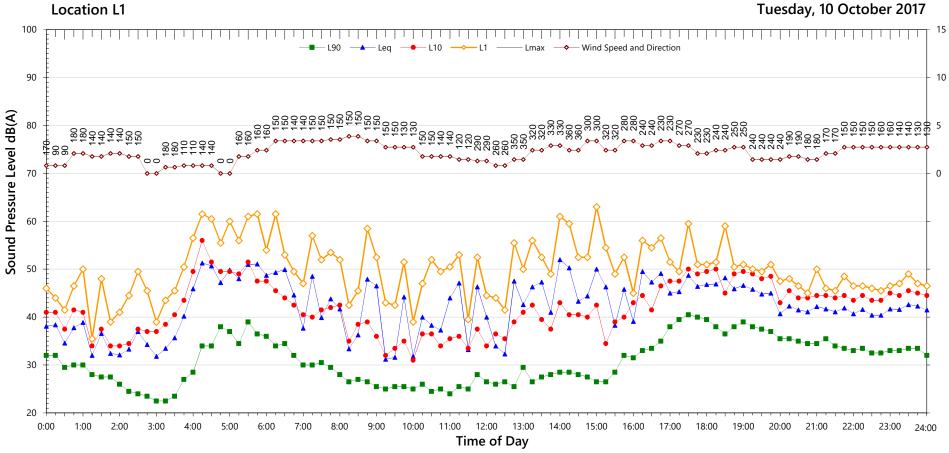
^{3. &}quot;Evening" is the period from 6pm till 10pm

^{4. &}quot;Night" relates to the remaining periods

^{5. &}quot;Night" relates to period from 10pm on this graph to morning on the following graph.

^{6.} Graphed data measured in free-field; tabulated results facade corrected

^{7.} Night time L_{Max} values are shown only where $L_{Max} > 65 dB(A)$ and where L_{Max} - Leq $\geq 15 dB(A)$



NSW Industrial Noise Policy (Free Field)			
Descriptor	Day ²	Evening ³	Night ^{4 5}
L ₉₀	25.0	33.5	30.0
LAeq	45.5	44.3	45.6

Night Time Maximur	n Noise Levels		(see note 7)
L _{Max} (Range)	-	to	-
L _{Max} - L _{eq} (Range)	-	to	-

NSW Road Noise Policy (1m	(see note 6)	
Descriptor	Day	Night⁵
Descriptor	7am-10pm	10pm-7am
L _{eq 15 hr} and L _{eq 9 hr}	47.7	48.1
L _{eq 1hr} upper 10 percentile	50.7	52.2
L _{ea 1hr} lower 10 percentile	42.4	43.4

Notes

Wind Speed (m/s)

^{1.} Shaded periods denote measurements adversely affected by rain, wind or extraneous noise - data in these periods are excluded from calculations.

^{2. &}quot;Day" is the period from 8am till 6pm on Sundays and 7am til 6pm on other days

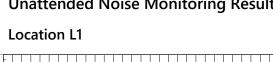
^{3. &}quot;Evening" is the period from 6pm till 10pm

^{4. &}quot;Night" relates to the remaining periods

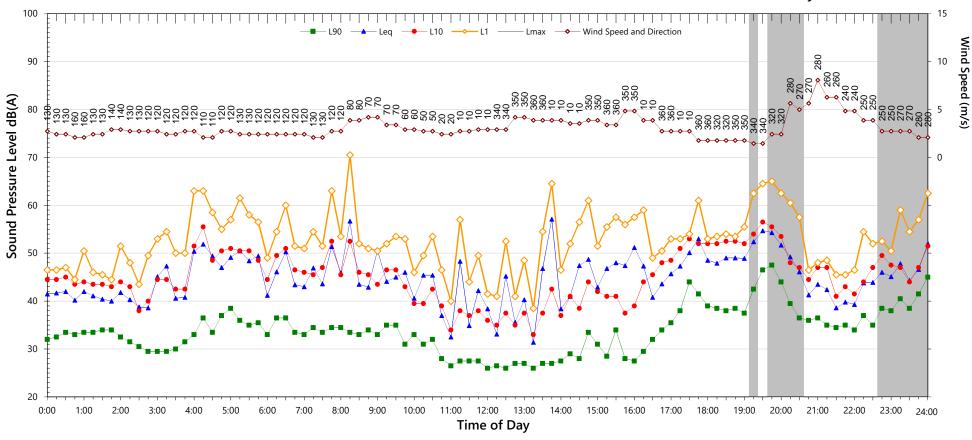
^{5. &}quot;Night" relates to period from 10pm on this graph to morning on the following graph.

^{6.} Graphed data measured in free-field; tabulated results facade corrected

^{7.} Night time L_{Max} values are shown only where $L_{Max} > 65 dB(A)$ and where L_{Max} - Leq $\geq 15 dB(A)$



Wednesday, 11 October 2017



NSW Industrial Noise Policy (Free Field)			
Descriptor	Day ²	Evening ³	Night ^{4 5}
L ₉₀	26.5	34.5	32.0
LAeq	48.0	47.9	42.4

Night Time Maximun	n Noise Levels		(see note 7)
L _{Max} (Range)	-	to	-
L _{Max} - L _{eq} (Range)	-	to	-

NSW Road Noise Policy (1n	(see note 6)	
Descriptor	Day	Night⁵
Descriptor	7am-10pm	10pm-7am
L _{eq 15 hr} and L _{eq 9 hr}	50.5	44.9
L _{eq 1hr} upper 10 percentile	56.0	46.4
L _{eq 1hr} lower 10 percentile	43.1	41.7

Notes:

^{1.} Shaded periods denote measurements adversely affected by rain, wind or extraneous noise - data in these periods are excluded from calculations.

^{2. &}quot;Day" is the period from 8am till 6pm on Sundays and 7am til 6pm on other days

^{3. &}quot;Evening" is the period from 6pm till 10pm

^{4. &}quot;Night" relates to the remaining periods

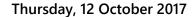
^{5. &}quot;Night" relates to period from 10pm on this graph to morning on the following graph.

^{6.} Graphed data measured in free-field; tabulated results facade corrected

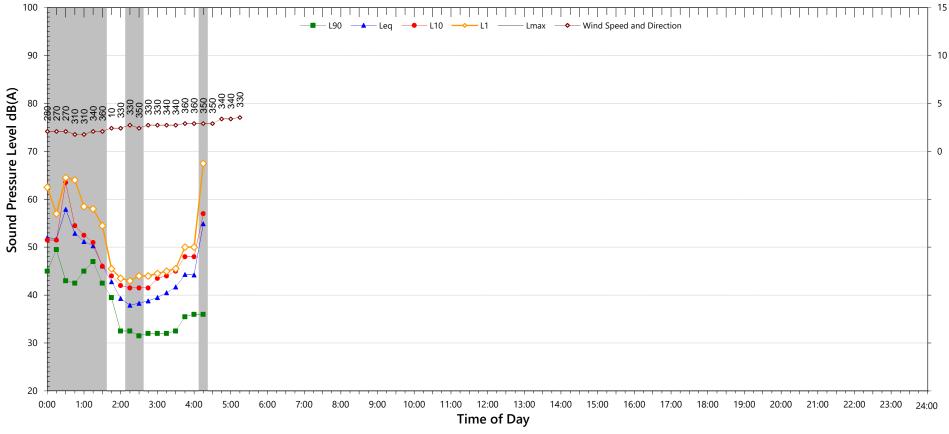
^{7.} Night time L_{Max} values are shown only where $L_{Max} > 65 dB(A)$ and where L_{Max} - Leq $\geq 15 dB(A)$

Location L1

onattended Noise Monitoring Results



Wind Speed (m/s)



NSW Industrial Noise Policy (Free Field)			
Descriptor	Day ²	Evening ³	Night ^{4 5}
L ₉₀	-	-	-
LAeq	-	-	-

Night Time Maximur	n Noise Levels		(see note 7)
L _{Max} (Range)	-	to	-
L _{Max} - L _{eq} (Range)	-	to	-

NSW Road Noise Policy (1m	(see note 6)	
Docarintor	Day	Night⁵
Descriptor	7am-10pm	10pm-7am
L _{eq 15 hr} and L _{eq 9 hr}	-	-
L _{eq 1hr} upper 10 percentile	-	-
L _{eq 1hr} lower 10 percentile	-	-

Notes

^{1.} Shaded periods denote measurements adversely affected by rain, wind or extraneous noise - data in these periods are excluded from calculations.

^{2. &}quot;Day" is the period from 8am till 6pm on Sundays and 7am til 6pm on other days

^{3. &}quot;Evening" is the period from 6pm till 10pm

^{4. &}quot;Night" relates to the remaining periods

^{5. &}quot;Night" relates to period from 10pm on this graph to morning on the following graph.

^{6.} Graphed data measured in free-field; tabulated results facade corrected

^{7.} Night time L_{Max} values are shown only where $L_{Max} > 65 dB(A)$ and where L_{Max} - Leq $\geq 15 dB(A)$